



TITLE:
TECHNICAL SPECIFICATION FOR
WET STACK FLOW MODEL STUDY
PROJECT: PVUNL-3X800MW PATRATU STPP
EXPANSION PHASE-1

SPEC. NO.: PE-TS-434-142-N102
VOLUME: I
SECTION:
REV. NO. 00 DATE 19.03.2019
SHEET 1 OF 12

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1.00.00 INTENT OF SPECIFICATION:

The intent of this enquiry/ specification is to carry out the Wet stack flow model study of **PVUNL-3X800MW PATRATU STPP EXPANSION PHASE-1** project for complete duct system from absorber outlet to the top of the stack, design and optimization of gas flow and liquid collection system to mitigate stack liquid discharge (SLD) and shell corrosion, Preparation of final report and recommendations, preparation of drawings/ documents for execution of collection system, obtaining approval on documents from BHEL/ Customer/ customer's consultant, Preparation of BOQ, preparation of bought out item specification, procurement assistance for specialized items, site visit as specified later in the specification & as necessary for completeness in all respects and for efficient & trouble free operation of chimney and liquid collection system for project.

2.00.00 SCOPE OF WORK:

Wet stack model study shall consist of the following:

- Condensation calculations & design of condensate collection system
- A scale physical flow model (Min. 1:12 scale) for liquid collector system (LCS) design.
- A computational flow model for plume downwash analysis.
- A physical or computational flow model for CEMS elevation flow performance.
- Design of optimum choke geometry if required.
- Review & Approval of liquid collector system construction drawings.
- Site inspection & supervision for 7 days to verify and evaluate LCS system performance prior to commissioning.

Wet stack study shall be performed for each unit with a wet stack installation where there does not exist an identical or mirror image installation. The objective of the wet stack study shall be to maximize liquid collection downstream of the mist eliminators and to preclude ground level rainout from the stack by recommending experimentally developed, tested, and optimized liquid collection devices and drainage systems to return collected liquid to the absorber with minimum re-entrainment.

The following codes and standard shall be followed for the conductance of this study:

- Revised wet stack design guidelines, 2012 by EPRI
- ACI 307 (American concrete institute code requirement for RC chimney
- EPRI report CS-2520 Entrainment in wet stack 1982
- EPRI report TR 107099 Wet stack design guide 1996
- EPRI report TR-109380 guidelines for fluid dynamic design of power plant ducts, 1998
- EPRI report GS-6984 FGD mist eliminator system design and specification guide
- CICIND, ICAC, US EPA and other international and other latest codes and standards.



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The study shall be carried out by design methods and tools:

- Preliminary design review based on experience
- Laboratory flow modeling -3-D
- Computer flow modelling -3-D
- Computer program calculations – 2-D

2.01.01 Preliminary design review based on experience

Based on the inputs furnished as per enclosed Annexure with this specification for the duct work and stack, preliminary design review need to be carried out to estimate the liquid collection requirements, predict the condensation rate in the duct & stack and perform the preliminary system design.

2.01.02 Condensation calculations using analytical / numerical tools

Gas flow study should include the calculation for the condensate formed and / or condensate carry over. The condensate flow study should include condensate quantity formed due to:

- i) Thermal condensation on the liners
- ii) Adiabatic condensation
- iii) Turbulence of flue gas flow near entry of the stack
- iv) At the outlet duct from absorber mist eliminator outlet
- v) Contribution from mist eliminator carryover in case of normal wash cycle or mist eliminator become fouled with time.

Detailed calculations along with the design basis for condensation rate in the duct from absorber outlet to the top of the chimney for the worst operating case, minimum boiler load and design conditions shall be furnished as a function of ambient air temperature, wind velocity and liner design variables in the report with an accuracy of $\pm 10\%$.

2.01.03 Design of Condensate collection & drainage system

- (i) Size of gutter(s) along with inner surface of Chimney flue can and inlet duct from absorber outlet to inlet of chimney flue can, such that condensate is collected efficiently and drained to FGD system.
- (ii) As the gutter shall be made of Titanium/C-276 as compatible with inner surface, suitable shape, size and thickness is to be recommended so that gas flow occurs efficiently.



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- (iii) The size, thickness, location and material of condensate drainage pipe shall be included in recommendation. It is envisaged that pipe from gutter to outside of Chimney liner shall be of Titanium/C-276 and thereafter the drainage pipe shall be of FRP leading to FGD system. Routing of the drain pipes shall be provided.

After the flow-model study is performed, accordingly design of liquid-collection devices for the full scale Wet Stack is to be carried out and detailed drawings, design basis and calculations shall be submitted.

2.01.04 Computational 3-D fluid-dynamic-model study (CFD Analysis)

Performance of a computational 3-D fluid-dynamic-model study of the minimum upper one third of the stack liner and shell to evaluate downwash of the wet plume. CFD model shall include the surrounding structure which are significant to wind/ plume flow patterns preferably minishell, external handrails and floor at the stack outlet.

A computational model of the stack shell and liner(s) shall be constructed for the plume downwash study. The plume downwash study shall include analysis of the local wind/temperature data to identify the occurrence of critical wind and temperature conditions. The plume downwash study shall identify the stack velocity and ambient wind conditions that produce downwash and the maximum extent of expected downwash throughout the year for shell corrosion protection. For sites where ambient temperatures reach freezing, a "winter" period shall be simulated to evaluate icing potential on the stack.

Depending on the results of the downwash study, there may be a need to develop an optimum choke geometry, if required, to minimize the plume downwash & liquid impingement of the shell. This includes evaluation of liquid collectors and drains to prevent re-entrainment and discharge of large droplets from the top of the choke.

Bidder to use the latest software for the CFD modelling and shall submit the model along with results in form of contours and vector plots of velocity, pressure, concentration and temperature at various test locations and summarized in tabular format. The model shall be tested with various simulated operating, minimum and design flow conditions, maximum wind speed, wind orientations, to evaluate the potential of the downwash.

The Bidder shall review Minishell details (Liner extension above roof) enclosed as an Annexure and confirm the liner-extension design with their recommendation.



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In case of the excessive downwash or reversed flow at stack exit or liquid exiting the stack liner and forming on the top of the concrete shell, bidder to provide the corrective actions, design modifications and evaluate the modified geometry.

2.02.00 Physical model of the system

An experimental gas-flow-model study to design and develop liquid collectors for the duct and stack downstream of the mist eliminator that will collect and drain liquid from the walls to prevent re-entrainment.

Laboratory Physical model study shall include the following details for wet stack design:

- i. Estimation of the total liquid load on the liner surface as a result of thermal and adiabatic condensation. This estimate shall be based on the liner and shell geometry, thickness, materials of construction and the flue gas-flow rate and properties over a range of expected plant-operating conditions and worst-case ambient weather conditions considering the mist eliminator fouling / wash cycles.
- ii. Design and optimization of liquid collectors in the absorber-outlet hood, absorber-outlet ducts, stack-liner entrance region and stack liner outlet to prevent SLD. The collectors will collect liquid from surfaces, re-entrainment, and guide the liquid to locations where it can be drained out of the system. This development work shall be conducted on a scale model of the wet duct and stack system, from the outlet of each absorber's mist eliminator include the absorber outlet and ducting, the stack breaching duct and a minimum of three (3) diameters of the stack liner above the top of the stack breaching duct. Model scales shall be minimum 1:12 and to be selected to ensure accurate modeling results for all tested parameters. The same shall be finalized after the award of the contract. The design should be of integrated complete system of liquid collectors from absorber outlet to chimney top for each unit.
- iii. The laboratory test includes details of liquid re-entrainment and drainage behavior over the expected range of unit operating conditions and confirm the stack-liner design velocity.
- iv. Physical model shall include any internal devices that may affect the gas flow, such as structural members, internal dampers, flow controls, and expansion joints. The model shall be mainly constructed from transparent acrylic or plastic, sheet metal, or coated rigid tubing such that it is suitable for wet testing. Modeled flow control and liquid collection devices may be constructed with sheet metal, or other suitable



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construction materials, so long as the scaled liquid flow performance is not adversely modified.

- v. The physical model shall be tested for pressure and velocity profiles at selected cross sections through the ducts and liner. A velocity traverse shall be conducted within the modeled liner to ensure that the cyclonic flow levels are within the U.S. EPA Method 1 recommended limitations for CEMS operation. In the event testing indicates that cyclonic flow could be a concern at the continuous emissions monitoring system (CEMS) elevation, a simulation, either by extension to the physical model or using a computational fluid dynamic model, shall be performed to evaluate this flow at the CEMS level. If needed, corrective devices shall be designed and tested to reduce stack swirl at the CEMS elevation.
- vi. The physical model shall be tested by introducing liquid in a size and quantity such that the model shall approximately match the two-phase flow modeling requirements for droplet trajectory and loading. This testing shall be used to locate and design the liquid collection devices and drains.
- vii. Evaluation of re-entrainment at liner-expansion joints in the laboratory test rig and development of a unit-specific liquid-collector geometry to collect and drain the liquid from the liner-expansion joints.
- viii. Using this model effective internal liquid collection devices shall be developed and optimized to improve the droplet deposition and liquid collection in the stack as well as to prevent the re-entrainment of droplets from liquid pools and films.
- ix. Bidder shall submit the detailed standard procedure for carrying out the physical model study at vendor lab for customer information / approval before the conductance of physical model study at lab.

2.03.00 Site inspection & supervision

Bidder to perform an onsite inspection as per the EPRI Revised Wet Stack Design Guideline, 2012. Site visit should occur for 7 days time during the construction phase, when liquid collection system is nearing completion, to inspect the liquid collection system as installed to ensure that the designed flow controls, liquid collectors, drains, and drain protection are installed properly and shall perform as intended. Bidder to provide the site inspection report to validate the design and installation.

The onsite inspection should confirm that the liquid-collection system has been fabricated and installed correctly and to identify any deviations to the recommended



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design as a result of field modifications made to ease installation. The bidder shall also ensure the liquid collection system is installed properly.

The key deliverables from this study are:

- a) Bidder to furnish the total quantity of condensate formed from absorber mist eliminator outlet to top of the stack.
- b) Bidder to furnish the number, sizing and location of required various liquid collectors/ gutters, their shape, design of its evacuation piping from inside the chimney to outside and their Influence on the flow in the chimney liner.
- c) Flow model study shall minimize system pressure losses and optimize collection and drainage and provide expected field wet stack system pressure loss across expected load range.
- d) Bidder to achieve minimum stack liquid discharge. In case of excessive stack liquid discharge, possible means of modification to duct and stack geometry need to be proposed by bidder for improvement.
- e) Bidder to ensure the design of effective liquid collection system for various plant load operating conditions and absorber combinations.
- f) Bidder to furnish the comparison of the experimental and computer modelling.
- g) Bidder to recommend modifications to prevent the chimney liquid discharge issues and to make the geometry more favorable for liquid collection.
- h) Bidder to furnish the fabrication/installation drawings after the completion of model study for fabrication.
- i) Bidder to identify appropriate liner system and gas inlet geometries (including flow control devices) to ensure homogeneous gas flow conditions and achieve cyclonic free flow distribution at the CEMS location.
- j) Bidder to provide recommendations and design for sealing drain piping/ seal pots to inhibit backflow.
- k) Bidder to recommend drain protection devices to minimize pluggage occurrences an flow and recommend method for monitoring liquid collection drainage flow in case of liquid collection system pluggage and SLD problems.
- l) Bidder to provide stack outlet modifications, such as liner extensions or chokes, to minimize stack icing occurrences and to provide Stack shell coating requirements to protect concrete shells from corrosion due to plume downwash.
- m) Bidder to evaluate the plume downwash and recommend modifications to minimize downwash using CFD model preferably at reduced unit load operation and high wind speed conditions.
- n) Bidder to provide the drawings/documents for the necessary provisions in Chimney during the course of this study, if applicable, to carry out the performance test for wet stack at site in future.



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2.04.00

Specific Technical Requirements

Wet stack sizing criteria:

- a) A "wet Chimney" shall be installed downstream of Wet Flue Gas Desulfurization (FGD) system. Clean gas from the absorber shall be taken to the Chimney through three stage mist eliminators. Treated flue gas from the absorber shall be discharged through a wet stack without reheating of the flue gas. In such a case the flue gas will be saturated. However, provision has also been made for isolation of the flue gas flow through the absorber and also for bypass of the absorber, to allow maintenance of the absorber with the unit in operation. In such a case flue gas will directly go to the Chimney after ID Fans through bypass duct.

The Contractor, shall take into account the entire characteristics of expected combination of fuels to be fired, for the complete load range of operation and the expected numbers of Steam Generator start-ups while designing the Chimney flue liner considering Steam Generator in operation both with & without FGD system in operation. The chimney flue liner cladding shall be made of 2 mm thick Titanium (Grade 2 as per ASME SB265) or C-276 alloy over 8 mm thick (minimum) mild steel base metal of flue liner. Cladding shall be done to achieve the required quality as per ASTM B 898-11. External surface of chimney flue liner projecting over the chimney roof shall be wrapped with 2 mm thick Titanium / C-276 sheet over insulation. The stack shall be designed as per the latest guidelines of EPRI Wet Stack Design Guide. The design of wet ducts and stacks system shall consider the Stack liquid discharge (SLD), Corrosion/chemical attack, Condensate collection system and its drainage etc.

Parameter	Units	Design point - Normal Operation with FGD in Operation	Design point- Operation with Bypass Operation
Flue gas quantity per boiler	T/Hr	4705.94	4338
Temp. of flue gas at stack inlet	°C	61.8	147
Flue gas density at stack inlet	Kg/m ³	1.00487	0.793
Volumetric flow per boiler	M ³ /s	1300.87	1519.55
Stack Height	M	275	275
Ambient air temp.	°C	45	45
Relative Humidity	%	60	60
Internal flue dia	M	9.9	9.9
Flue gas velocity at stack exit	m/sec	16.8	19.7

- b) A wet stack study shall be performed by the Contractor for each unit with a wet stack installation where there does not exist an identical or mirror image installation that has already had a wet stack study performed. A wet stack model study shall consist of the following:



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- (i) Condensation calculations
- (ii) Minimum 1:12 scale physical flow model for liquid collector design
- (iii) Computation flow model for plume downwash analysis
- (iv) Physical or computation flow model for CEMS elevation flow performance

c) Liquid collectors shall be designed and developed experimentally using a physical model. The model shall begin at the outlet of the absorber mist eliminator(s), include the absorber outlet and ducting, the stack breaching duct and a minimum of three (3) diameters of the stack liner above the top of the stack breaching duct. Physical model shall include any internal devices that may affect the gas flow, such as structural members, flow controls, and expansion joints. Liquid collectors shall be located where needed in the absorber outlet, the ductwork between the absorber outlet and the wet stack liner, in the wet stack liner, and in the exit nozzle. These collectors shall collect liquid from surfaces, prevent re-entrainment, and guide the liquid to location where it can be drained out of the system and prevent the discharge of droplets from the top of the stack that are large enough to rain out to the ground before evaporation.

2.05.00 GENERAL

- a) Bidder to furnish the detailed Master drawing list for wet stack flow model study for BHEL and customer approval.
- b) Bidder to provide technical advice/ recommendations/ assistance & solutions regarding site related construction problems related to condensate collection and drainage system in the duct and chimney as and when required including site visits, participation in meetings through VC/WEB with BHEL/ customer/ customer's consultant.
- c) The physical model study may be witnessed by BHEL / Plant Owner for approximately 3 days. Intimation for the witnessing shall be provided by the bidder 4 weeks prior to conductance of physical model test at vendor lab. Video streaming facility shall also be provided for witnessing the physical model test from India. In addition, complete physical model test including the flow patterns and droplets trajectory shall be recorded on video CD which shall be provided after the physical model study.
- d) The physical model shall be stored at the vendor lab at no cost for a period of 1 year after the submission of final report and completion of the study. Thereafter its further disposal or storage shall be decided after the award of the contract on the cost basis. Optional prices may be quoted for the same and this shall not be considered for the evaluation of bid.



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- e) The bidder is advised to take care all information that may be necessary for preparing the bid and entering into the contract. Claims of any kind due to variation or ignorance of site conditions and environmental conditions after award of works will not be entertained.
- f) All revisions/changes required as per BHEL/ Project owners, comments/ requirements, site requirement etc. shall be carried out by the bidder.
- g) Three hard copies of approved reports/documents/drawings shall be submitted by the bidder. Electronic copies of the CFD model, analysis and report shall be submitted in primary original format as well as in printable non-proprietary formats (e.g. .pdf).
- h) Change in recommendation / design after the analysis shall be taken care by bidder without any commercial implication in this contract value.
- i) Bidder shall furnish detailed activity schedule, report generation schedule and list of inputs required for successful execution of Wet stack flow model study.
- j) The Purchaser/ Customer however also reserve the rights to check the detailed calculations in the event of order and their interpretation shall be final in the event of any conflict.
- k) Bidder shall furnish all the documents in English and SI units shall also be followed in the calculations and reports wherever used.

3.00.00 DELIVERY SCHEDULE

Bidder has to carry out the complete activity including physical model, CFD, drawing /documents and final report approval by BHEL and plant owner within 15 weeks from the date of purchase order.

4.00.00 SUGGESTIVE DRAWINGS/ DOCUMENTS SUBMISSION:

Following Basic drawings/documents to be submitted within 2 weeks from LOI date.

1. MASTER DRAWING /DOCUMENT LIST. (to be finalized after order)
2. WET STACK STUDY SCHEDULE, PLANNING AND MILESTONES
3. LIST OF CODES AND STANDARDS TO BE FOLLOWED.



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4. DETAILED STANDARD PROCEDURE FOR PHYSICAL MODEL & CFD STUDY, DRAWINGS & DOCUMENTS SUBMISSION.
5. DESIGN DRAWINGS OF CONDENSATE COLLECTION AND DRAINAGE SYSTEM
6. THERMAL AND ADIABATIC CONDENSATION CALCULATIONS WITH DESIGN BASIS

Following Basic drawings/documents to be submitted and duly approved within 15 weeks from LOI date.

1. TECHNICAL DATASHEETS
2. BILL OF QUANTITIES
3. WET STACK STUDY REPORT WITH RECOMMENDATIONS
4. CFD MODEL, ANALYSIS AND RESULTS

This is not an exhaustive list of drawings/ documents for WET STACK STUDY.

Bidder shall furnish all applicable drawings /documents other than as mentioned above which is/are required for successful execution of condensate collection and drainage system after the absorber outlet to stack outlet.

NOTE:

1. Subsequent revisions of above drgs/docs to be submitted within 7 days of comments received from BHEL/ CUSTOMER.
2. Drawings submitted shall be complete in all respects with revised drawing submitted incorporating all comments. Any incomplete drawing submitted shall be treated as non-submission with delays to bidder's account.

5.00.00 DOCUMENTS TO BE SUBMITTED ALONG WITH BID

- a) Detailed procedure adopted for the conductance of the study.
- b) Wet stack study planning and scheduling.
- c) Computer program to be used for the 3D modelling and analysis.
- d) Mathematical tools & codes / programs used for the analytical calculations.
- e) Technical deviation schedule (if reqd.) (enclosed herein)

Apart from above no other drawings/documents/data sheets etc. are required to be submitted at bid stage and even if furnished shall not be taken cognizance of.



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6.00.00 SALIENT TECHNICAL POINTS:

1. Maximum mist carryover from mist eliminator -20 mg/NM3
2. The droplet size distribution of the mist after the mist eliminator (ME) – 100% Droplet size less than 40 microns.
3. Expected mist carryover from mist eliminator during on load washing cycle – 20 mg/Nm3
4. Layout from absorber outlet to chimney inlet is identical for all the three units. Therefore, study will be conducted for 1 unit only. FGD layout details are provided in Annexure-V for performing the model study

ANNEXURE-I

PVUNL-2X800MW PATRATU STPP



PROJECT INFORMATION

EPC PACKAGE FOR
PATRATU SUPER THERMAL POWER STATION
EXPANSION PHASE-1 (3x800 MW)

TECHNICAL SPECIFICATION
SECTION-VI, PART-A
BID DOC NO: CS-9585-001-2

CLAUSE NO.	PROJECT INFORMATION																
1.00.00 2.00.00 3.00.00 4.00.00 4.01.00 4.02.00 4.03.00	PATRATU STPS EXPANSION PHASE-I (3X800 MW) BACKGROUND A Memorandum of Agreement (MOA) has been entered on 29.07.2015 amongst Govt. of Jharkhand (GoJ), Jharkhand Urja Vikash Nigam Limited (JUVNL), Jharkhand UrjaUtpadan Nigam Limited (JUUNL), Jharkhand BijliVitaran Nigam Limited (JBVNL) and NTPC Limited to form a Joint Venture Company of NTPC Limited & JBVNL for transfer of Patratu Thermal Power Station (PTPS) located in Ramgarh District of Jharkhand State to the proposed JV Company for Performance Improvement of existing capacity & 4000 MW Capacity expansion of PTPS. Further to signing of JV agreement on 29.07.2015, a Joint Venture Company namely Patratu Vidyut Utpadan Nigam Limited (PVUNL) has been incorporated amongst GoJ, JUVNL, JBVNL and NTPC Ltd. on 15.10.2015. The Performance Improvement of existing capacity and 4000 MW Capacity expansion of Patratu STPS will be implemented by the JV Company (JVC). The configuration of expansion of 4000 MW shall consist of 5 units of 800 MW to be implemented in two phases; Phase-I: 3x800 MW and Phase-II: 2x800 MW. The present proposal is for Patratu STPS Phase-I (3x800 MW). The project is envisaged to be commissioned during XIII Plan period. CAPACITY Patratu STPS Phase-I: 3x800 MW - Present proposal MODE OF OPERATION Base Load LOCATION AND APPROACH Patratu Thermal Power station (PTPS) is located just outside the coal belt of South Karanpura in Ramgarh District of Jharkhand State. The nearest Railway Station is Patratu which is at a distance of about 4 km on Barkakhana-Barwadih Railway line. The latitudes and longitudes of the site are as follows: <table border="1" data-bbox="400 1485 1201 1693"> <thead> <tr> <th>Corner name</th><th>Latitude</th><th>Longitude</th></tr> </thead> <tbody> <tr> <td>Top Corner</td><td>23° 38 ' 60 '' N</td><td>85° 17' 51.5" E</td></tr> <tr> <td>Bottom Corner</td><td>23° 38 ' 12.5 '' N</td><td>85° 17' 27" E</td></tr> <tr> <td>Left Corner</td><td>23° 38 ' 22.5 '' N</td><td>85° 17' 10.6 '' E</td></tr> <tr> <td>Right Corner</td><td>23° 38 ' 40 '' N</td><td>85° 17' 57 '' E</td></tr> </tbody> </table> Airport The nearest commercial airport is Ranchi at about 45 km by road.	Corner name	Latitude	Longitude	Top Corner	23° 38 ' 60 '' N	85° 17' 51.5" E	Bottom Corner	23° 38 ' 12.5 '' N	85° 17' 27" E	Left Corner	23° 38 ' 22.5 '' N	85° 17' 10.6 '' E	Right Corner	23° 38 ' 40 '' N	85° 17' 57 '' E	
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Left Corner	23° 38 ' 22.5 '' N	85° 17' 10.6 '' E															
Right Corner	23° 38 ' 40 '' N	85° 17' 57 '' E															
EPC PACKAGE FOR PATRATU SUPER THERMAL POWER STATION EXPANSION PHASE-I (3X800 MW)	TECHNICAL SPECIFICATION SECTION – VI, PART-A BID DOC. NO CS-9585-001-02	SUB-SECTION-IB PROJECT INFORMATION															

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CLIMATOLOGICAL TABLE

जलवायु सारणी
CLIMATOLOGICAL TABLE

स्टेशन : रामगढ़
STATION : Ramgarh

STATION: Ramgerh

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ANNEXURE-II

DATA FOR CHIMNEY DESIGN

GENERAL DATA									
Boiler Application		Utility		No. of Chimneys		By PEM			
Boiler Capacity		800 MW		Type of Chimney		By PEM			
No. of Boilers		Three (03)		Chimney Arrangement		By PEM			
Fuels Fired		Coal		Height of Chimney		By PEM			
OPERATING CONDITIONS (Per Boiler) – FGD Outlet Parameters									
DESCRIPTION / LOAD		Chimney Design Point		FGD Design Point		FGD Guarantee Point			
		BMCR 25% EA		VWO 25% EA		TMCR 25% EA			
		Worst Coal		Worst Coal		Worst Coal			
Flue Gas Flow	t / h	4705.94		4590.05		4240.01			
Flue Gas Volume	m ³ / s (wet)	1300.87		1271.10		1141.77			
Flue Gas Temperature	°C	61.8		62.1		58.1			
Flue Gas Density	kg / m ³	1.00487		1.00308		1.03154			
FGD OUTLET-FLUE GAS COMPOSITION % BY VOLUME – (WET BASIS)									
CO ₂		9.26		9.23		9.67			
N ₂		63.88		63.68		66.62			
O ₂		5.68		5.67		5.91			
SO ₂		0.0023		0.0023		0.0021			
H ₂ O		21.18		21.42		17.79			
Customer / Plant: NTPC-Patratu (3x800MW)									
Prop. No.:		Rev. 0		Rev. 1		Rev. 2		Rev. 3	
		Sign	Date	Sign	Date	Sign	Date	Sign	Date
Engineer : Raju P		RP	10-04-18	YR	07-06-18				
Reviewer : Shaktikanta Dash		SKD	10-04-18	SKD	07-06-18				
Approver : Lakshmanan R		RL	10-04-18	RL	07-06-18				



DATA FOR CHIMNEY DESIGN AT FGD OUTLET FOR PAR LOADS - PATRATU

GENERAL DATA								
Boiler Application		Utility						
Boiler Capacity		800 MW						
No. of Boilers		Three (03)						
Fuels Fired		Coal						
OPERATING CONDITIONS (Per Boiler)								
DESCRIPTION / LOAD		40%-TMCR		50%-TMCR		40%-TMCR		50%-TMCR
		Design Coal		Design Coal		Worst Coal		Worst Coal
Flue Gas Flow t / h		1818.26		2276.10		1846.80		2260.60
Flue Gas Volume m ³ / s (wet)		484.78		608.78		501.69		611.43
Flue Gas Temperature °C		57.10		56.50		59.80		58.90
Flue Gas Density kg /m ³		1.0418		1.043		1.0225		1.027
FGD OUTLET-FLUE GAS COMPOSITION % BY WEIGHT – (WET BASIS)								
CO ₂		10.59		10.03		10.22		9.89
N ₂		67.06		67.40		65.53		66.10
O ₂		5.32		6.06		4.96		5.49
SO ₂		0.0022		0.0027		0.0024		0.0027
H ₂ O		17.02		16.48		19.28		18.49
Customer / Plant: NTPC-Patratu (3x800MW)								
Prop. No.:		Rev. 0		Rev. 1		Rev. 2	Rev. 3	
	Sign	Date	Sign	Date	Sign	Date	Sign	Date
Engineer :								
Reviewer :								
Approver :								

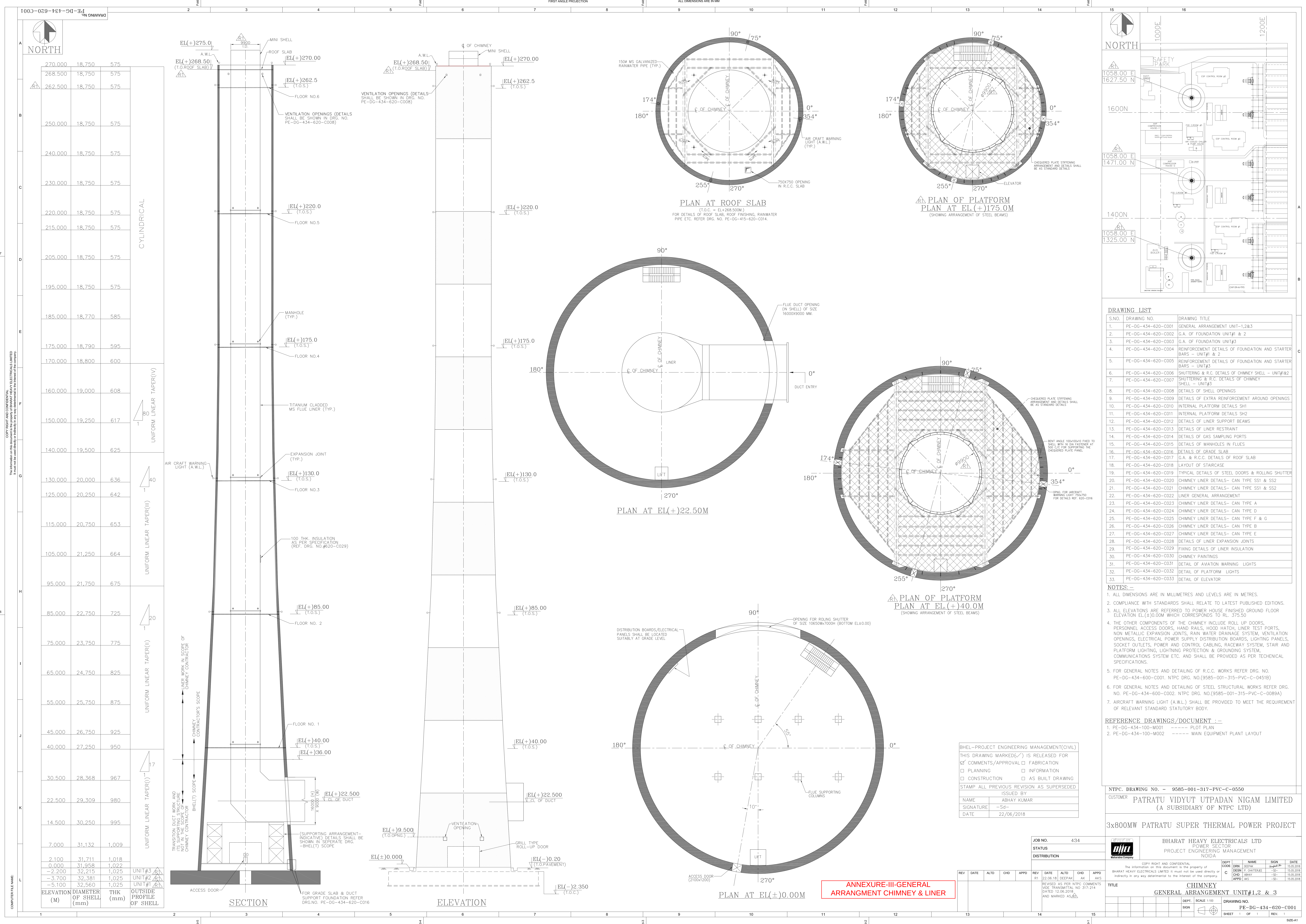
ANNEXURE-II

PVUNL/ PATRATU STPS Expansion, Phase – I, 3x800 MW
Cont No : 1828-1830

Rev 00
Date 05/06/2018

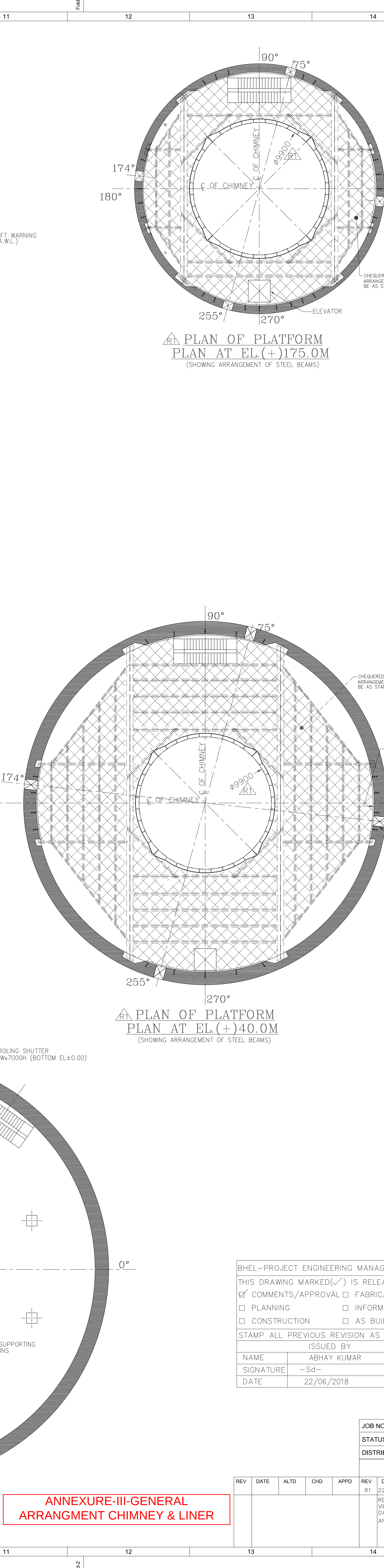
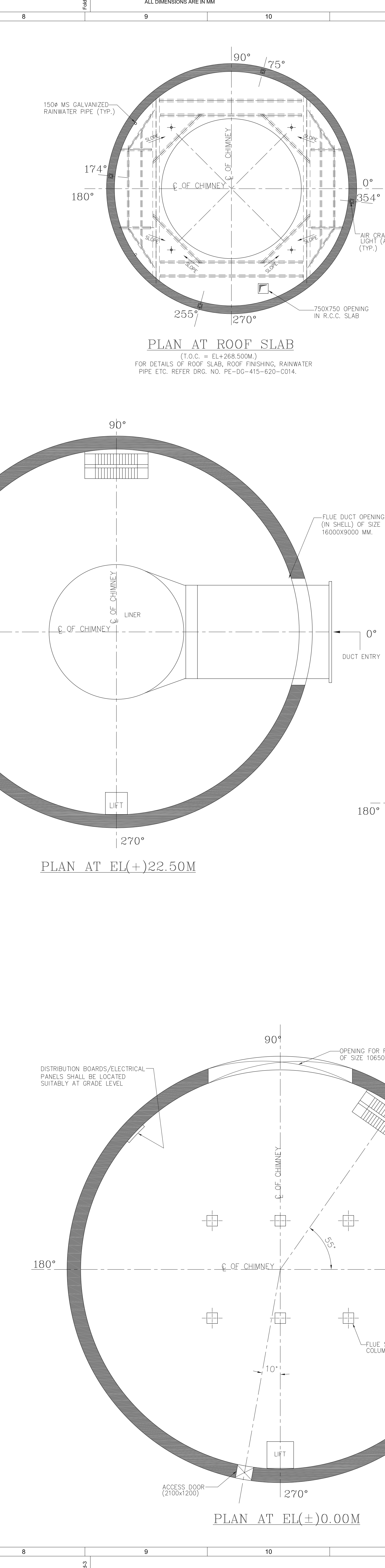
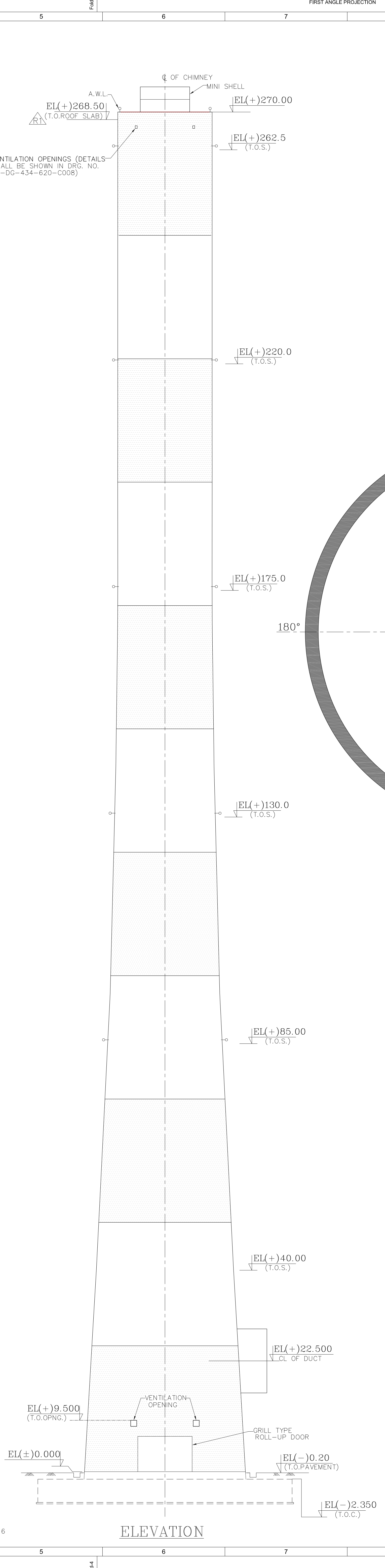
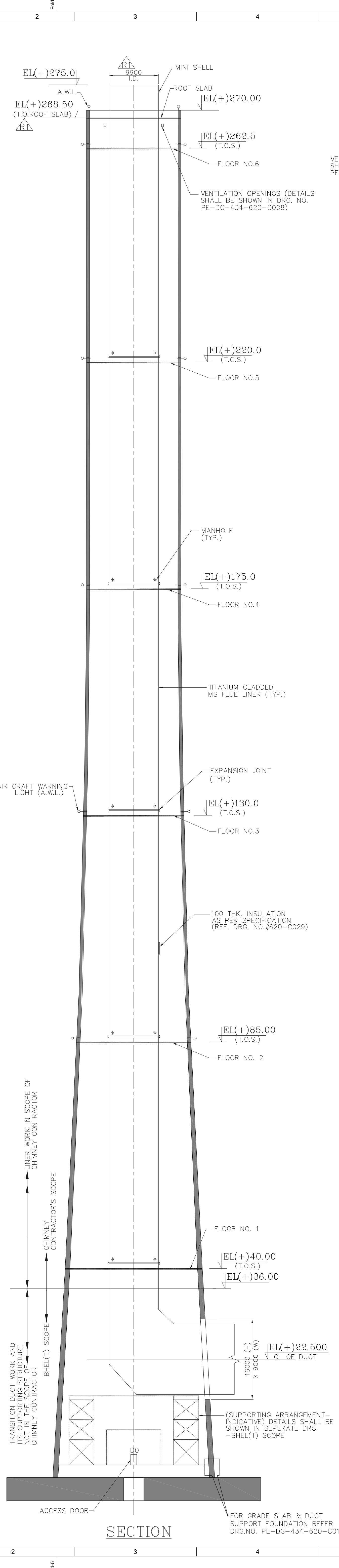
Chimney Selection data

			FGD Bypass
S.No.	Description	Unit	BMCR WC, 25%EA, 45degC Design Point
1	Ambient Temperature	Deg C	45
2	Excess Air	%	25
3	Relative Humidity	%	60
4	Heat Duty	MKcal/kg	1662
5	Efficiency	%	83.97
6	Q Fired	Mkcal/hr	1980
7	Coal Quantity	t/hr	683
8	Air Quantity	t/hr	3365
9	Gas quantity entering APH	t/hr	3759
10	AH leakage	%	12.00
11	AH leakage	t/hr	451
12	Gas quantity Leaving APH	t/hr	4210
13	Gas temperature Leaving APH	Deg C	147
14	Duct Leakage	%	2
15	Gas quantity entering ESP	t/hr	4295
16	ESP leakage	%	1
17	Gas quantity leaving ESP	t/hr	4338
19	Gas quantity entering Chimney	t/hr	4338
20	Gas temperature entering Chimney	Deg C	147
21	Density	kg/m ³	0.793
22	Volume of Gas	m ³ /s	1520
23	FLUE GAS ANALYSIS AT CHIMNEY INLET (WET BASIS)		
A	CARBON-DI-OXIDE	%	15.74
B	SULPHUR-DI-OXIDE	%	0.28
C	OXYGEN	%	6.38
D	NITROGEN	%	67.35
E	MOISTURE	%	10.25



COMPUTER FILE NAME:			
PE-DG-434-620-C001			
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CYLINDRICAL			
270.000	18.750	575	
268.500	18.750	575	
262.500	18.750	575	
250.000	18.750	575	
240.000	18.750	575	
230.000	18.750	575	
220.000	18.750	575	
215.000	18.750	575	
205.000	18.750	575	
195.000	18.750	575	
185.000	18.770	585	
175.000	18.790	595	
170.000	18.800	600	
160.000	19.000	608	
150.000	19.250	617	
140.000	19.500	625	
130.000	20.000	636	
125.000	20.250	642	
115.000	20.750	653	
105.000	21.250	664	
95.000	21.750	675	
85.000	22.750	725	
75.000	23.750	775	
65.000	24.750	825	
55.000	25.750	875	
45.000	26.750	925	
40.000	27.250	950	
30.500	28.368	967	
22.500	29.309	980	
14.500	30.250	995	
7.000	31.132	1,009	
2.100	31.711	1,018	
0.000	31.958	1,022	
-2.200	32.215	1,025	
-3.700	32.381	1,025	
-5.100	32.560	1,025	
ELEVATION (M)	DIAMETER OF SHELL (mm)	THK (mm)	
UNIT#3			
UNIT#2			
UNIT#1			
OUTSIDE PROFILE OF SHELL			



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ELEVATION OF CAN TYPE 'SS2'

SECTION 2-2

DETAIL AT 'A'

DETAIL AT - 'F'

DETAIL AT - 'E'

SECTION 1-1

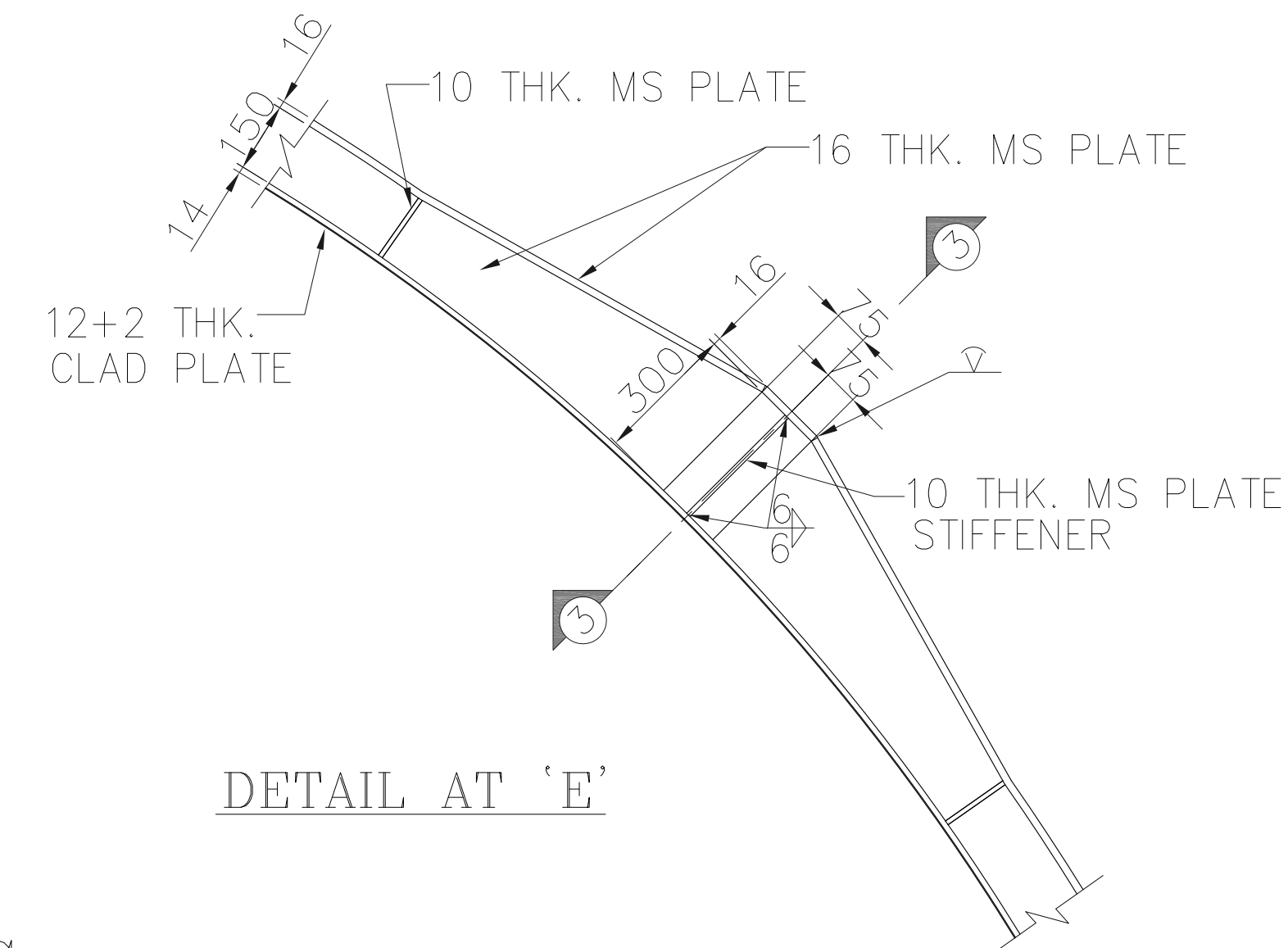
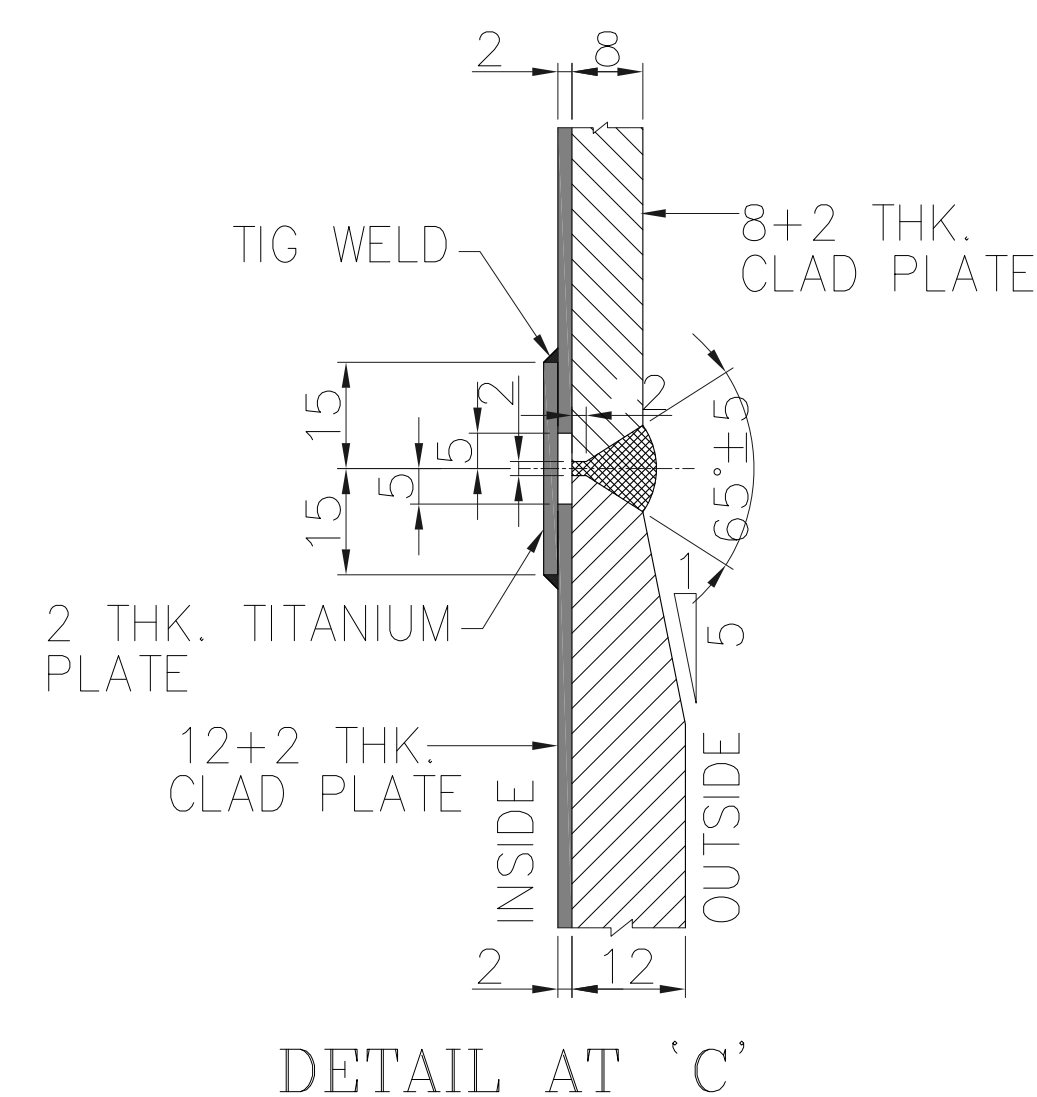
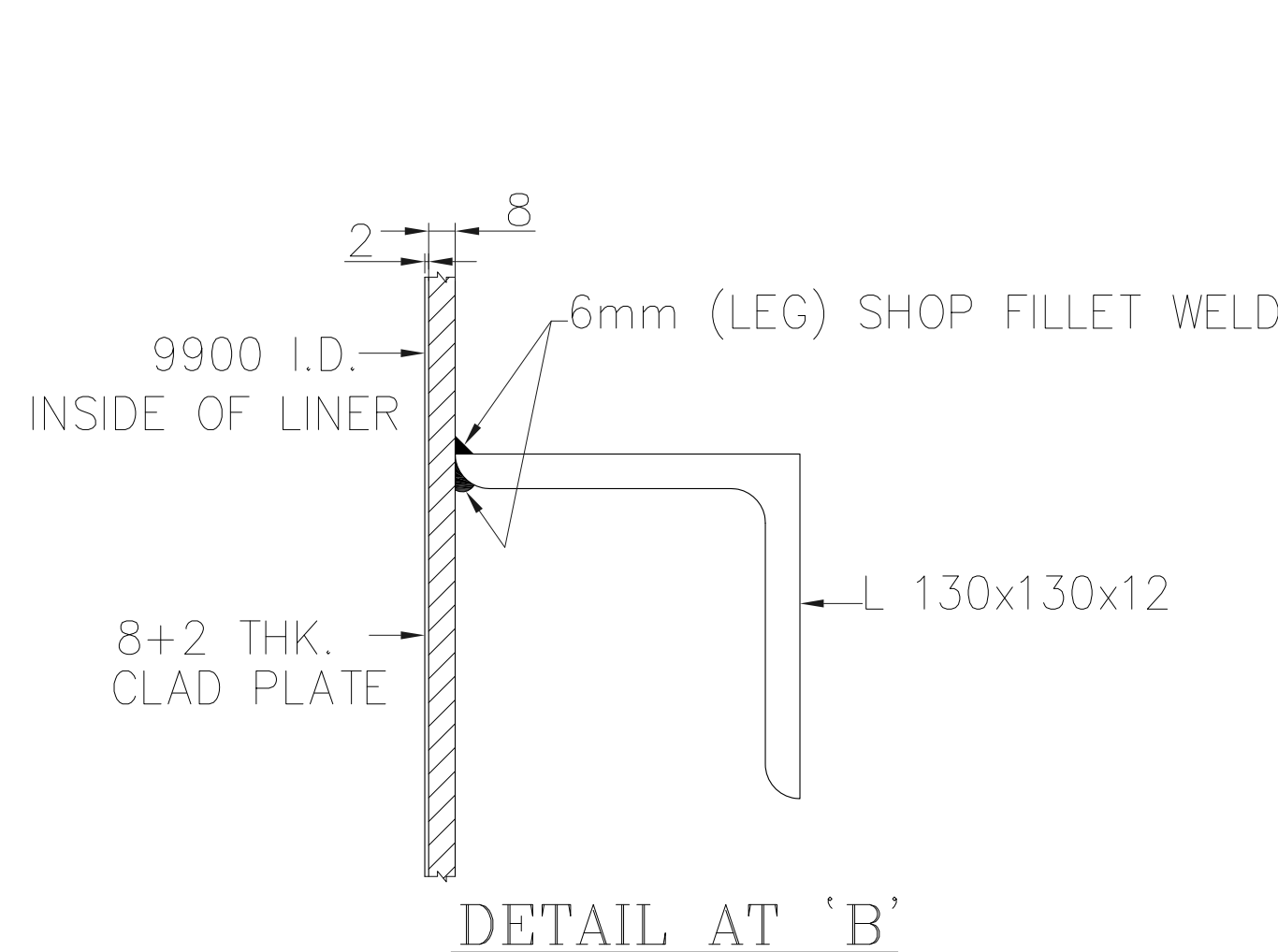
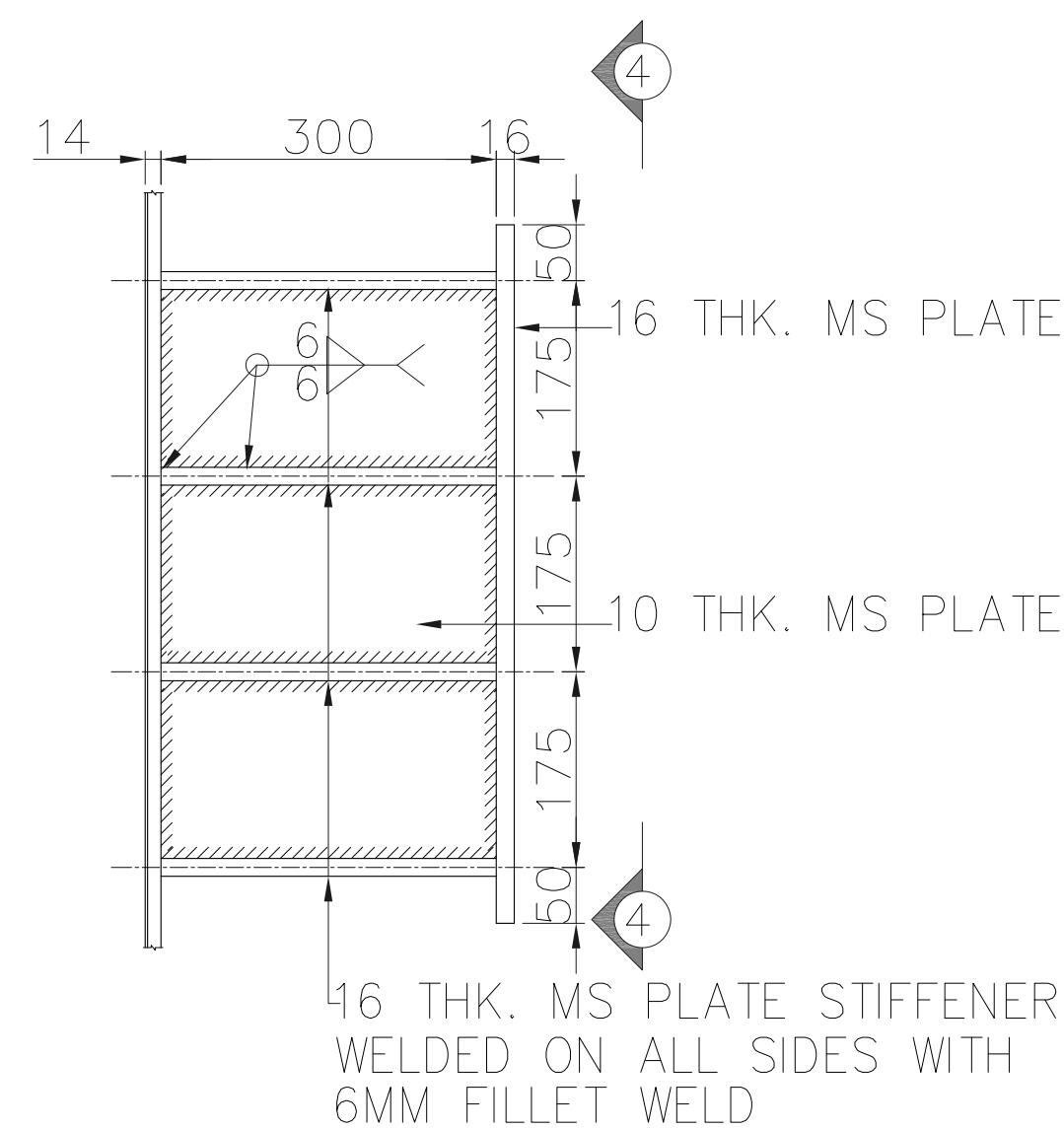
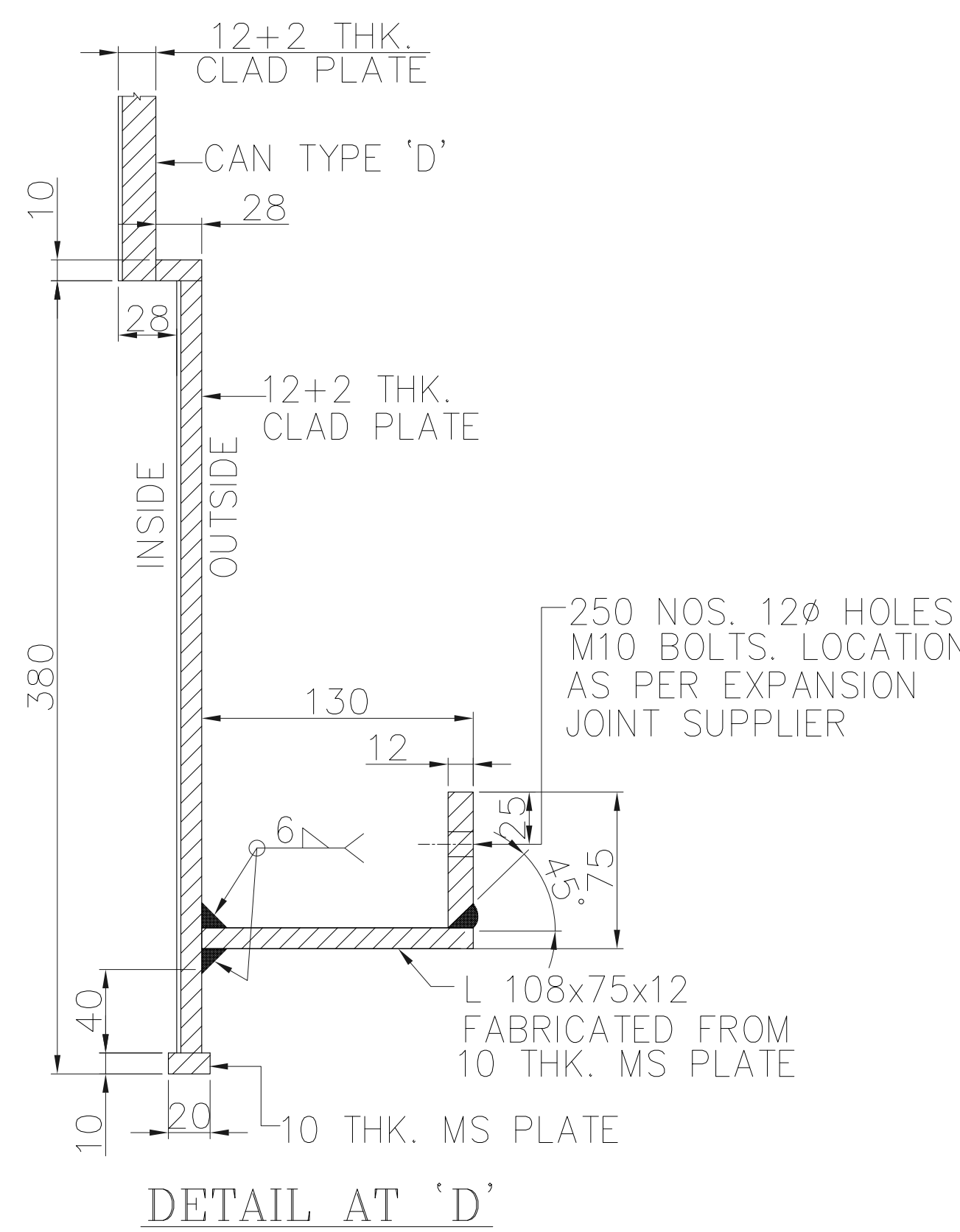
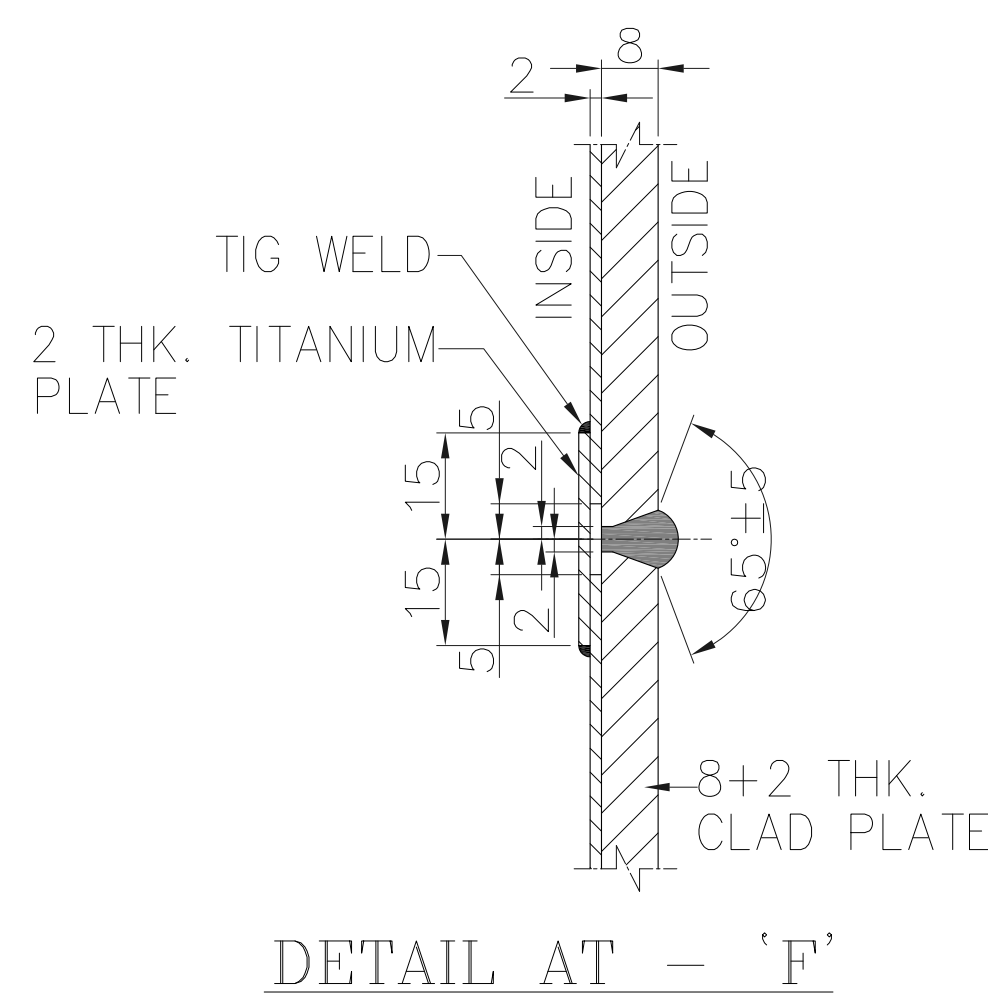
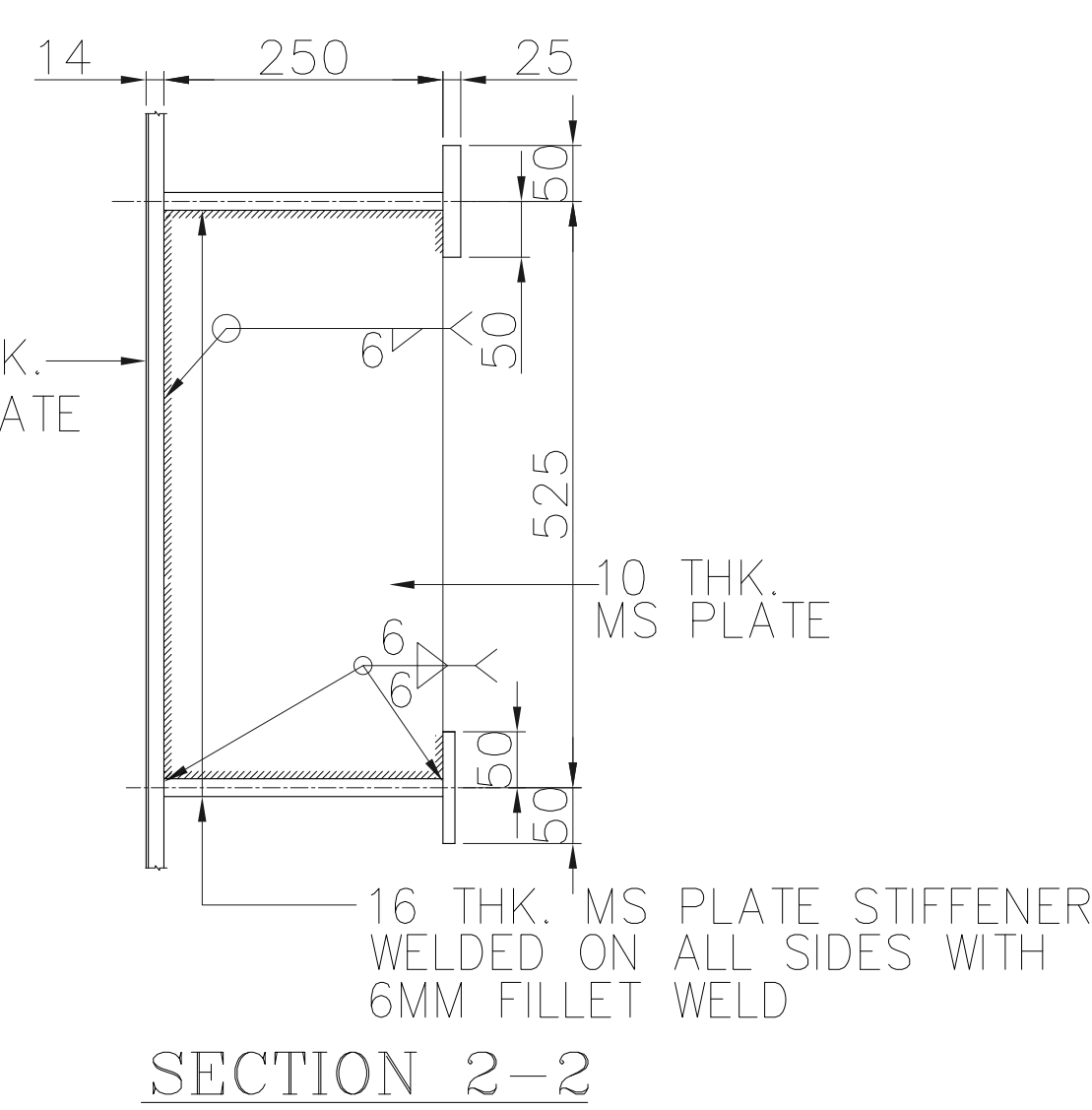
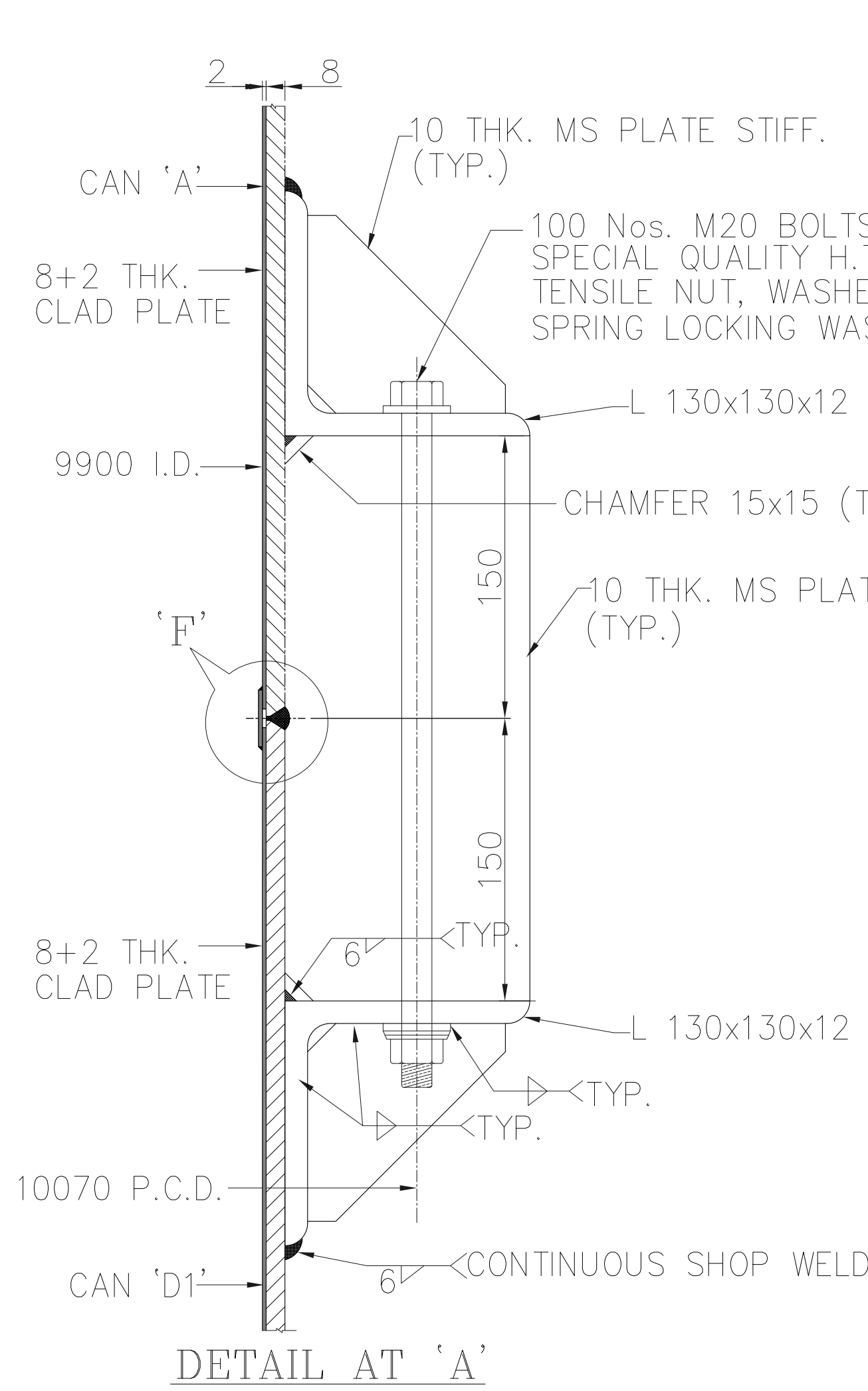
DETAIL AT 'B'

DETAIL AT 'C'

DETAIL AT - 'D'

1. ALL DIMENSIONS ARE IN MILLIMETERS. FIGURED DIMENSIONS SHALL BE FOLLOWED.
2. MILD STEEL PLATES AND ROLLED SECTIONS SHALL CONFIRM TO GRADE A OF IS:2062 FOR MATERIALS UPTO 20MM IN THICKNESS.
3. HOT ROLLED SECTIONS SHALL CONFIRM TO IS:808 PART I TO IV.
4. TITANIUM CLAD PLATES SHALL BE OF GRADE 2 AS PER ASME SB265 AND SHALL CONFORM TO ASTM B898-11. FABRICATION OF TITANIUM CLAD PLATES SHALL BE DONE IN ACCORDANCE WITH SPECIFICATION NO. 9591-001-317-PVC-U-400
5. SPECIAL QUALITY BOLTS SHALL BE BLACK GRADE OF PROPERTY CLASS 8.8 CONFIRMING IS:1367.
6. WASHERS, NUTS AND HELICAL SPRING LOCKING WASHERS SHALL BE OF QUALITY CLASS NOT LESS THAN THAT OF THE BOLTS.
7. WELDING FOR ALL MS. PLATE/MEMBERS SHALL BE DONE WITH LOW HYDROGEN TYPE WELDING CONFORM TO IS:816 NAD IS:9595 AND TO THE REQUIREMENT OF THE SPECIFICATION.
8. ALL FILLET AND BUTT WELDS ARE TO BE CONTINUOUS.
9. ALL SHOP WELDS USED TO CONNECT CURVED PLATES FORMING FLUE CANS AND OTHER BUTT WELDS, WHERE REQUIRED, SHALL BE FULL PENETRATION BUTT WELD.
10. ANY TEMPORARY STIFFENING STEEL WORK REQUIRED DURING FABRICATION, TRANSPORTATION OR ERECTION PURPOSES SHALL BE DESIGNED AND SUPPLIED BY THE CONTRACTOR, SUCH STEEL WORK SHALL BE REMOVED AND FLUE SURFACES MADE GOOD AFTER ERECTION.
11. TESTING OF WELDS UNLESS NOTED OTHERWISE ON THE DRAWINGS, SHALL BE AS FOLLOWS:
 - a) FILLET WELDS:
 - i) MACROETCH EXAMINATION ON PRODUCTION COUPONS.
 - ii) 100% DYE PENETRATION TEST/MAGNETIC PARTICLE TEST.
 - b) BUTT WELDS:
 - i) 100% DYE PENETRATION TEST AFTER BLACK GOUGING.
 - ii) 10% (FOR SHOP WELDS) AND 15% (FOR SITE WELDS) RADIOGRAPHY TEST. WHERE RADIOGRAPHY IS NOT POSSIBLE, ULTRASONIC TESTING WILL BE CARRIED OUT.
 - c) THE WELD RUN TO BE TESTED, SHALL BE EVENLY DISTRIBUTED OVER THE TOTAL LENGTH OF APPLICABLE WELDS ON EACH CAN.
 - d) THE PERCENTAGE OF WELDS TESTED, SHALL BE INCREASED AS JUDGED NECESSARY BY THE ENGINEER-IN-CHARGE, BUT TO NOT LESS THAN 20% FOLLOWING IDENTIFICATION OF SIGNIFICANT DEFECTIVE WELDS AND ONLY REDUCED TO THE 10%/15% NORM AFTER CONSISTENT QUALITY/INTEGRITY IS RE-ESTABLISHED.
12. WELDING OF TITANIUM PLATE SHALL BE DONE IN ACCORDANCE WITH TECHNICAL SPECIFICATION.
13. THE TERM 'SHOP' WELD REFERS TO ALL WELDS MADE DURING FABRICATION, OF INDIVIDUAL FLUE CANS AT FABRICATION YARD. 'SITE' WELD REFERS TO WELDS MADE DURING FLUE ERECTION FOR JOINING TOGETHER OF CANS WITHIN WIND SHIELD.
14. FOR GENERAL NOTES AND DETAILING OF STEEL STRUCTURAL WORKS REFER DRG. NO. PE-DG-434-600-C002.
15. CONDENSATE COLLECTION CHANNEL SHALL BE WELDED WITH FLUE CAN AS APPLICABLE AS PER CONDENSATE FLOW STUDY. FOR DETAIL AND LOCATION OF CONDENSATE COLLECTION CHANNEL REFER SEPARATE DRG.

SIZE-A1



1. ALL DIMENSIONS ARE IN MILLIMETERS. FIGURED DIMENSIONS SHALL BE FOLLOWED.
2. MILD STEEL PLATES AND ROLLED SECTIONS SHALL CONFIRM TO GRADE A OF IS:2062 FOR MATERIALS UPTO 20MM IN THICKNESS.
3. HOT ROLLED SECTIONS SHALL CONFIRM TO IS:808 PART I TO IV.
4. TITANIUM CLAD PLATES SHALL BE OF GRADE 2 AS PER ASME SB265 AND SHALL CONFORM TO ASTM B898-11. FABRICATION OF TITANIUM CLAD PLATES SHALL BE DONE IN ACCORDANCE WITH SPECIFICATION NO. 9591-102-315-PVC-U-0550F-03.
5. SPECIAL QUALITY BOLTS SHALL BE BLACK GRADE OF PROPERTY CLASS 8.8 CONFIRMING IS:1367.
6. WASHERS, NUTS AND HELICAL SPRING LOCKING WASHERS SHALL BE OF QUALITY CLASS NOT LESS THAN THAT OF THE BOLTS.
7. WELDING FOR ALL MS. PLATE/MEMBERS SHALL BE DONE WITH LOW HYDROGEN TYPE WELDING CONFORM TO IS:816 NAD IS:9595 AND TO THE REQUIREMENT OF THE SPECIFICATION.
8. ALL FILLET AND BUTT WELDS ARE TO BE CONTINUOUS.
9. ALL SHOP WELDS USED TO CONNECT CURVED PLATES FORMING FLUE CANS AND OTHER BUTT WELDS, WHERE REQUIRED, SHALL BE FULL PENETRATION BUTT WELD.
10. ANY TEMPORARY STIFFENING STEEL WORK REQUIRED DURING FABRICATION, TRANSPORTATION OR ERECTION PURPOSES SHALL BE DESIGNED AND SUPPLIED BY THE CONTRACTOR, SUCH STEEL WORK SHALL BE REMOVED AND FLUE SURFACES MADE GOOD AFTER ERECTION.
11. TESTING OF WELDS UNLESS NOTED OTHERWISE ON THE DRAWINGS, SHALL BE AS FOLLOWS:
 - a) FILLET WELDS:
 - i) MACROETCH EXAMINATION ON PRODUCTION COUPONS.
 - ii) 100% DYE PENETRATION TEST/MAGNETIC PARTICLE TEST.
 - b) BUTT WELDS:
 - i) 100% DYE PENETRATION TEST AFTER BLACK GOUGING.
 - ii) 10% (FOR SHOP WELDS) AND 15% (FOR SITE WELDS) RADIOGRAPHY TEST. WHERE RADIOGRAPHY IS NOT POSSIBLE, ULTRASONIC TESTING WILL BE CARRIED OUT.
 - c) THE WELD RUN TO BE TESTED. SHALL BE EVENLY DISTRIBUTED OVER THE TOTAL LENGTH OF APPLICABLE WELDS ON EACH CAN.
 - d) THE PERCENTAGE OF WELDS TESTED SHALL BE INCREASED AS JUDGED NECESSARY BY THE ENGINEER-IN-CHARGE, BUT TO NOT LESS THAN 20% FOLLOWING IDENTIFICATION OF SIGNIFICANT OF DEFECTIVE WELDS AND ONLY REDUCED TO THE 10/15% NORM AFTER CONSISTENT QUALITY/INTEGRITY IS RE-ESTABLISHED.
12. WELDING OF TITANIUM PLATE SHALL BE DONE IN ACCORDANCE WITH TECHNICAL SPECIFICATION.
13. THE TERM 'SHOP' WELD REFERS TO ALL WELDS MADE DURING FABRICATION, OF INDIVIDUAL FLUE CANS AT FABRICATION YARD. 'SITE' WELD REFERS TO WELDS MADE DURING FLUE ERECTION FOR JOINING TOGETHER OF CANS WITHIN WIND SHIELD.
14. FOR GENERAL NOTES AND DETAILING OF STEEL STRUCTURAL WORKS REFER DRG. NO. PE-DG-434-600-C002.
15. CONDENSATE COLLECTION CHANNEL SHALL BE WELDED WITH FLUE CAN AS APPLICABLE AS PER CONDENSATE FLUE STUDY. FOR DETAIL AND LOCATION OF CONDENSATE COLLECTION CHANNEL REFER SEPARATE DRG.
16. GAS SAMPLING PORT SHALL BE PROVIDED AS PER IN FLUE CAN AS PER DRG NO.#620-C014

NTPC. DRAWING NO. - 9585-001-317-PVC-C-0561

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NTPC

NTPC LIMITED

3x800MM PATRATU SUPER THERMAL POWER PROJECT

**Bharat Heavy
Electricals Company**

BHARAT HEAVY ELECTRICALS LTD
POWER SECTOR
PROJECT ENGINEERING MANAGEMENT
NOIDA

DEPT CODE	NAME	SIGN	DATE
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ORN	DESIGN	<-->	20.11.2017
CHD	LIBRARY	<-->	20.11.2017
APP	CHECKED	<-->	20.11.2017

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TITLE

CHIMNEY

LINER DETAILS- CAN TYPE D1

DEPT. SCALE : 1:500

SEEN

DRAWING NO.

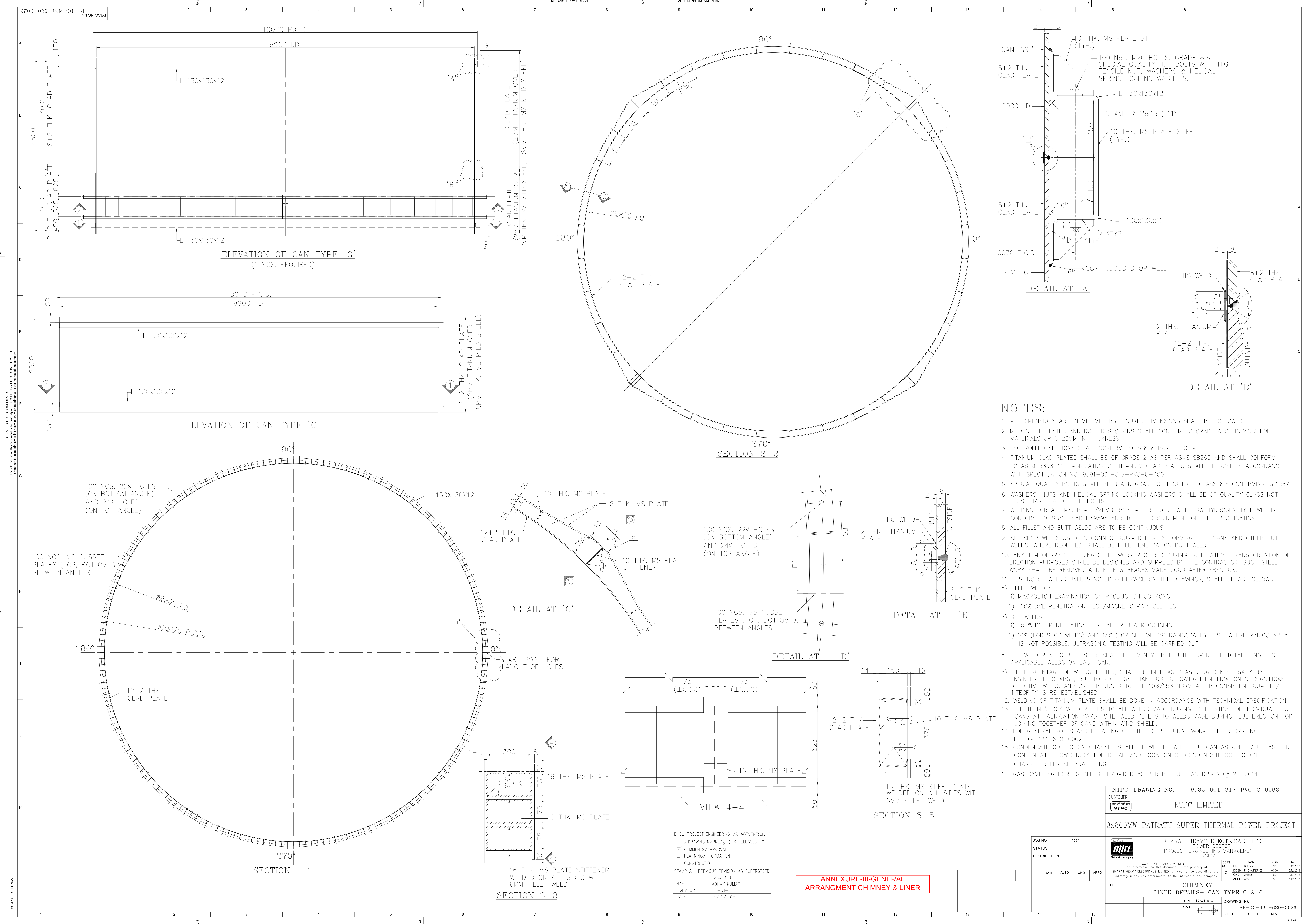
PE-DG-434-62D-C02

SHEET 1 OF 1 REV. 0

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			DESN P. CHATTERJEE	~S~	20.11.11
			CHD ASHAY	~S~	20.11.11
			APPD AKS	~S~	20.11.11

TITLE						<u>CHIMNEY</u>							
						<u>LINER DETAILS- CAN TYPE D1</u>							
						DEPT.		SCALE 1:100		DRAWING NO.			
						SIGN				PE-DG-434-620-CO24			
										SHEET 1 OF 1 REV. 0			

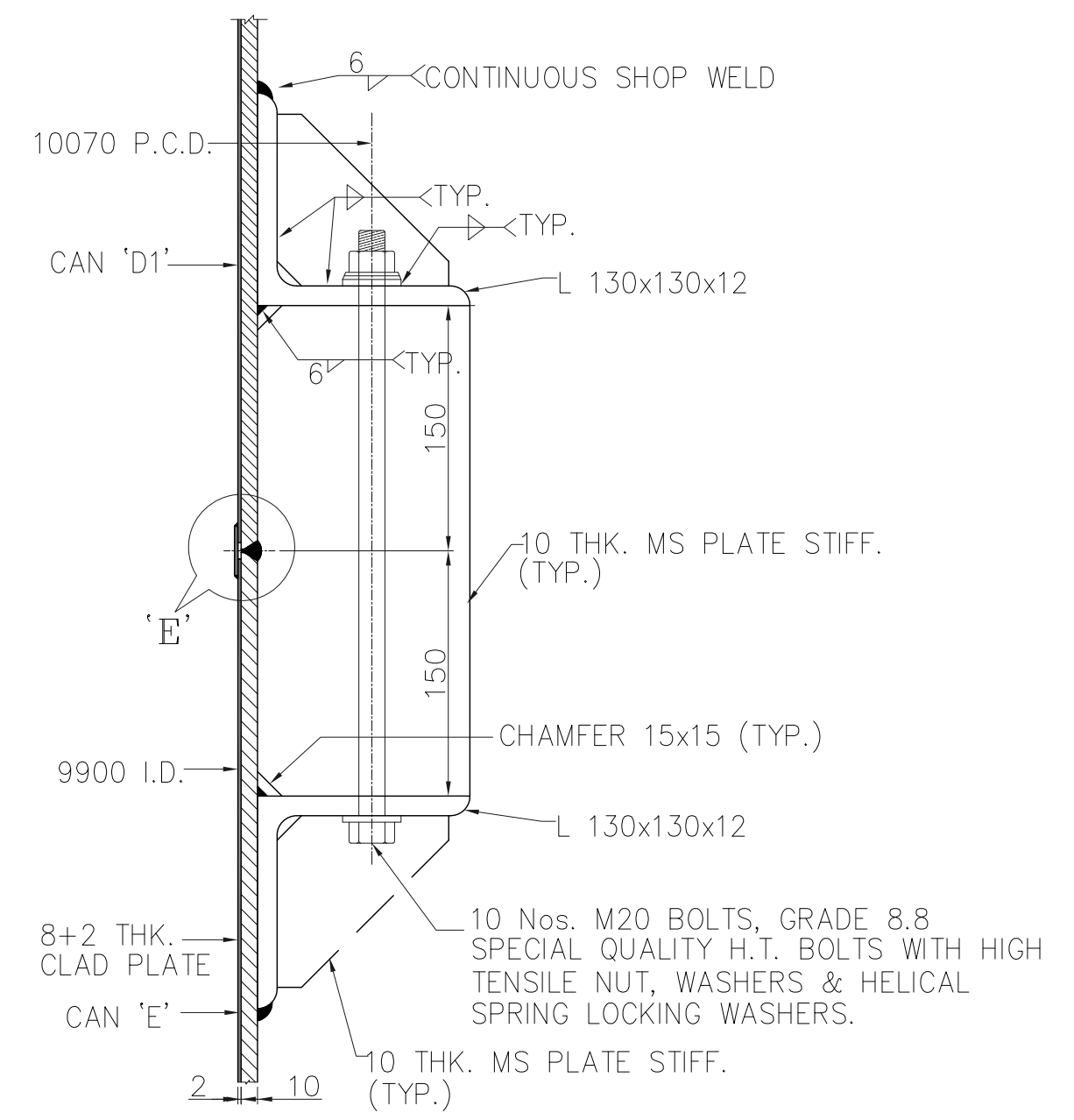
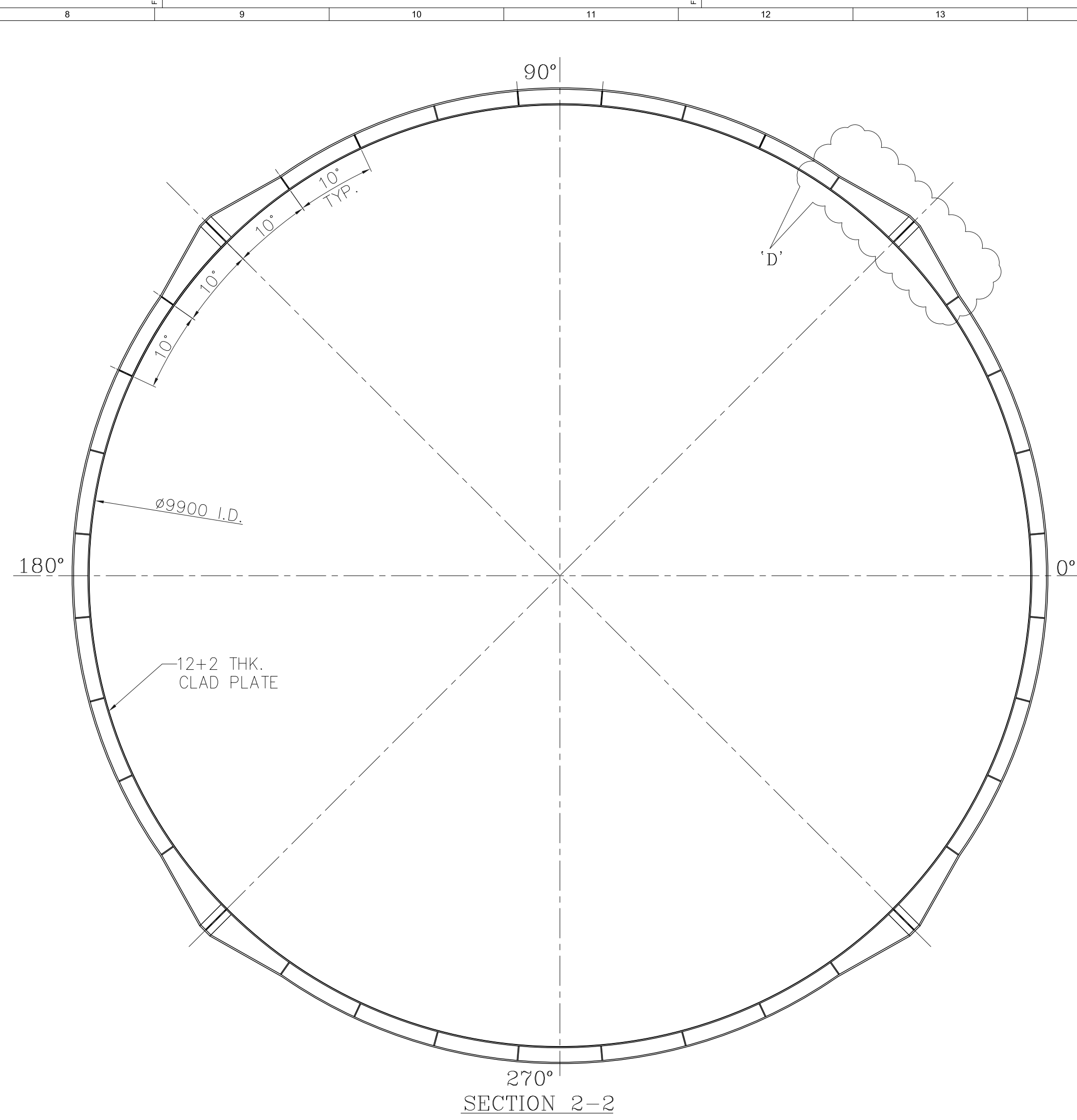
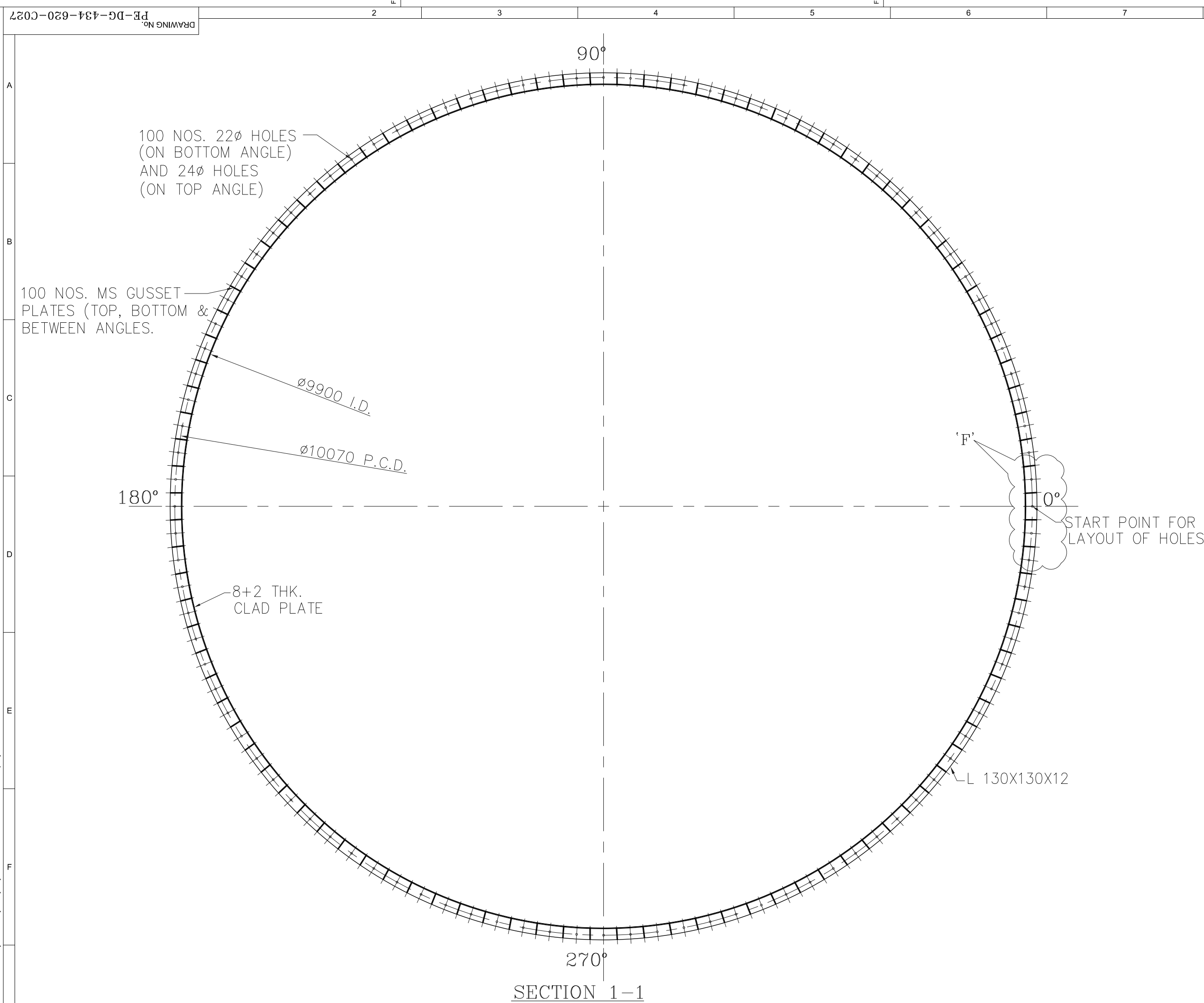


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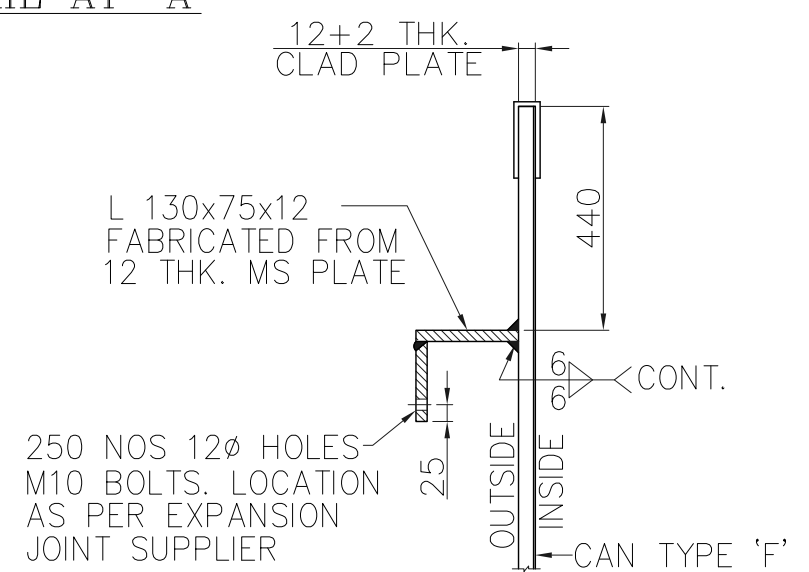
- ALL DIMENSIONS ARE IN MILLIMETERS. FIGURED DIMENSIONS SHALL BE FOLLOWED.
- MILD STEEL PLATES AND ROLLED SECTIONS SHALL CONFORM TO GRADE A OF IS:2062 FOR MATERIALS UPTO 20MM IN THICKNESS.
- HOT ROLLED SECTIONS SHALL CONFORM TO IS:808 PART I TO IV.
- TITANIUM CLAD PLATES SHALL BE OF GRADE 2 AS PER ASME SB265 AND SHALL CONFORM TO ASTM B898-11. FABRICATION OF TITANIUM CLAD PLATES SHALL BE DONE IN ACCORDANCE WITH SPECIFICATION NO. 9591-001-317-PVC-U-400
- SPECIAL QUALITY BOLTS SHALL BE BLACK GRADE OF PROPERTY CLASS 8.8 CONFIRMING IS:1367.
- WASHERS, NUTS AND HELICAL SPRING LOCKING WASHERS SHALL BE OF QUALITY CLASS NOT LESS THAN THAT OF THE BOLTS.
- WELDING FOR ALL MS. PLATE/MEMBERS SHALL BE DONE WITH LOW HYDROGEN TYPE WELDING CONFORM TO IS:816 NAD IS:9595 AND TO THE REQUIREMENT OF THE SPECIFICATION.
- ALL FILLET AND BUTT WELDS ARE TO BE CONTINUOUS.
- ALL SHOP WELDS USED TO CONNECT CURVED PLATES FORMING FLUE CANS AND OTHER BUTT WELDS, WHERE REQUIRED, SHALL BE FULL PENETRATION BUTT WELD.
- ANY TEMPORARY STIFFENING STEEL WORK REQUIRED DURING FABRICATION, TRANSPORTATION OR ERECTION PURPOSES SHALL BE DESIGNED AND SUPPLIED BY THE CONTRACTOR, SUCH STEEL WORK SHALL BE REMOVED AND FLUE SURFACES MADE GOOD AFTER ERECTION.
- TESTING OF WELDS UNLESS NOTED OTHERWISE ON THE DRAWINGS, SHALL BE AS FOLLOWS:
 - FILLET WELDS:
 - MACROETCH EXAMINATION ON PRODUCTION COUPONS.
 - 100% DYE PENETRATION TEST/MAGNETIC PARTICLE TEST.
 - BUT WELDS:
 - 100% DYE PENETRATION TEST AFTER BLACK COUGING.
 - 10% (FOR SHOP WELDS) AND 15% (FOR SITE WELDS) RADIOGRAPHY TEST. WHERE RADIOGRAPHY IS NOT POSSIBLE, ULTRASONIC TESTING WILL BE CARRIED OUT.
- THE WELD RUN TO BE TESTED, SHALL BE EVENLY DISTRIBUTED OVER THE TOTAL LENGTH OF APPLICABLE WELDS ON EACH CAN.
- THE PERCENTAGE OF WELDS TESTED, SHALL BE INCREASED AS JUDGED NECESSARY BY THE ENGINEER-IN-CHARGE, BUT TO NOT LESS THAN 20% FOLLOWING IDENTIFICATION OF SIGNIFICANT DEFECTIVE WELDS AND ONLY REDUCED TO THE 10%/15% NORM AFTER CONSISTENT QUALITY/INTEGRITY IS RE-ESTABLISHED.
- WELDING OF TITANIUM PLATE SHALL BE DONE IN ACCORDANCE WITH TECHNICAL SPECIFICATION.
- THE TERM 'SHOP' WELD REFERS TO ALL WELDS MADE DURING FABRICATION, OF INDIVIDUAL FLUE CANS AT FABRICATION YARD. 'SITE' WELD REFERS TO WELDS MADE DURING FLUE ERECTION FOR JOINING TOGETHER OF CANS WITHIN WIND SHIELD.
- FOR GENERAL NOTES AND DETAILING OF STEEL STRUCTURAL WORKS REFER DRG. NO. PE-DG-434-600-C002.
- CONDENSATE COLLECTION CHANNEL SHALL BE WELDED WITH FLUE CAN AS APPLICABLE AS PER CONDENSATE FLOW STUDY. FOR DETAIL AND LOCATION OF CONDENSATE COLLECTION CHANNEL REFER SEPARATE DRG.
- GAS SAMPLING PORT SHALL BE PROVIDED AS PER IN FLUE CAN DRG NO.#620-C014

NTPC. DRAWING NO. - 9585-001-317-PVC-C-0563			
CUSTOMER			
NTPC LIMITED			
3x800MW PATRATU SUPER THERMAL POWER PROJECT			
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TITLE CHIMNEY LINER DETAILS- CAN TYPE C & G			
DEPT. SCALE 1:100 SIGN			
DRAWING NO. PE-DG-434-620-C026			
SHEET 1 OF 1 REV. 0			

ANNEXURE-III-GENERAL
ARRANGMENT CHIMNEY & LINER



DETAIL AT 'A'

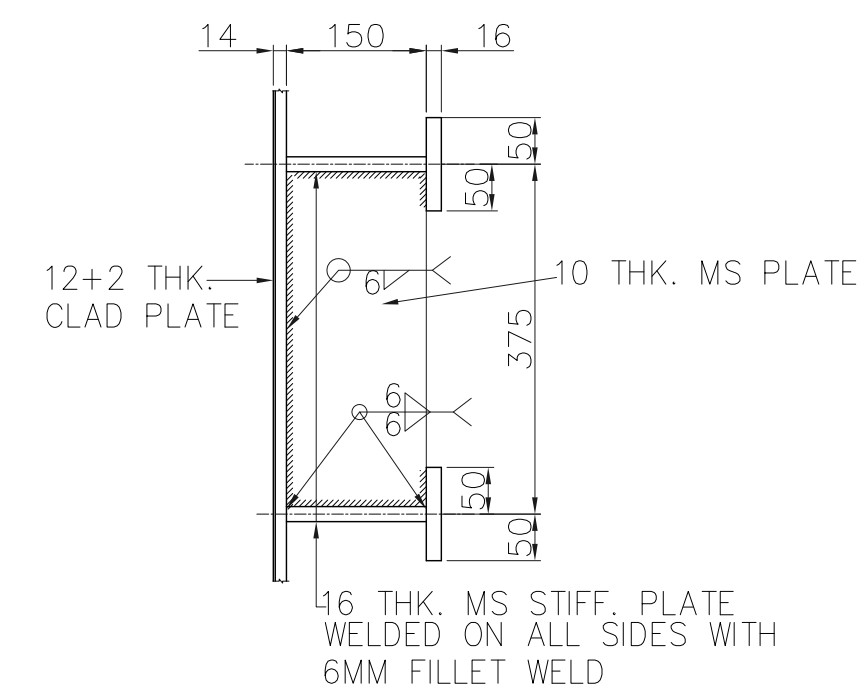


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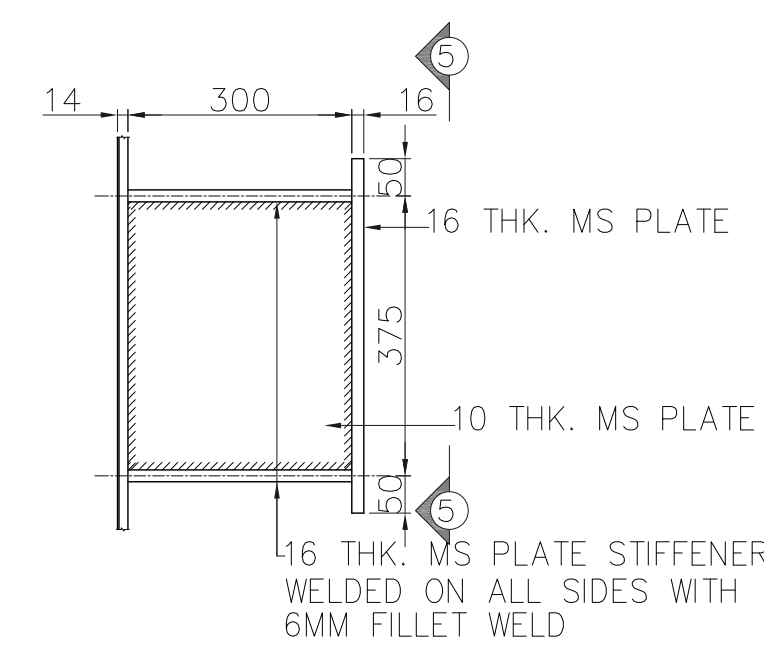
PART OF EXPANSION JOINT FOR DETAIL
REFER DRG. NO. PE-DG-434-620-C028
(NTPC DRG. NO. 9585-001-317-PVC-C-5081)

NOTES:—

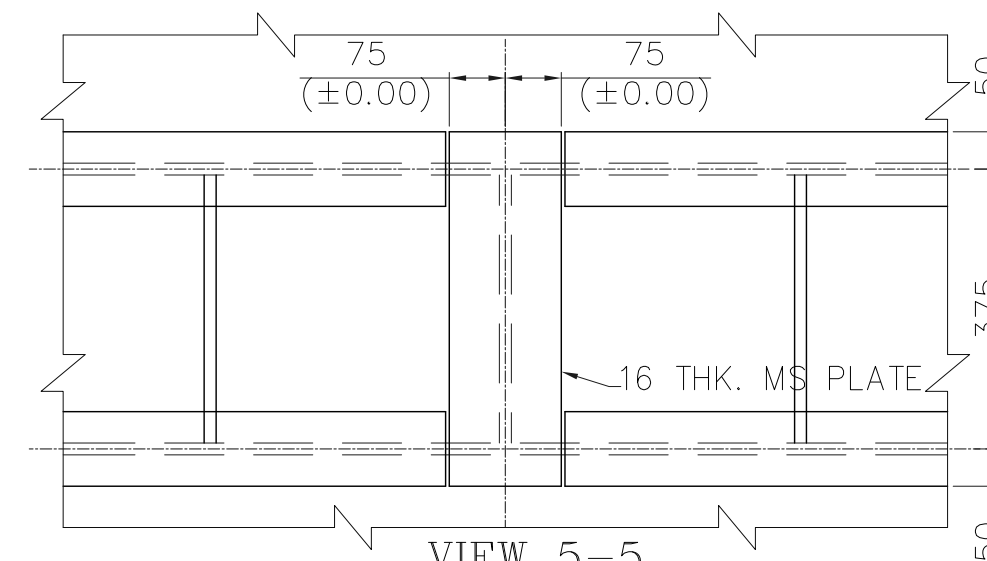
1. ALL DIMENSIONS ARE IN MILLIMETERS. FIGURED DIMENSIONS SHALL BE FOLLOWED.
2. MILD STEEL PLATES AND ROLLED SECTIONS SHALL CONFORM TO GRADE A OF IS:2062 FOR MATERIALS UPTO 20MM IN THICKNESS.
3. HOT ROLLED SECTIONS SHALL CONFORM TO IS:808 PART I TO IV.
4. TITANIUM CLAD PLATES SHALL BE OF GRADE 2 AS PER ASME SB265 AND SHALL CONFORM TO ASTM B898-11. FABRICATION OF TITANIUM CLAD PLATES SHALL BE DONE IN ACCORDANCE WITH SPECIFICATION NO. 9585-001-317-PVC-U-400.
5. SPECIAL QUALITY BOLTS SHALL BE BLACK GRADE OF PROPERTY CLASS 8.8 CONFIRMING IS:1367.
6. WASHERS, NUTS AND HELICAL SPRING LOCKING WASHERS SHALL BE OF QUALITY CLASS NOT LESS THAN THAT OF THE BOLTS.
7. WELDING FOR ALL MS. PLATE/MEMBERS SHALL BE DONE WITH LOW HYDROGEN TYPE WELDING CONFORM TO IS:816 NAD IS:9595 AND TO THE REQUIREMENT OF THE SPECIFICATION.
8. ALL FILLET AND BUTT WELDS ARE TO BE CONTINUOUS.
9. ALL SHOP WELDS USED TO CONNECT CURVED PLATES FORMING FLUE CANS AND OTHER BUTT WELDS, WHERE REQUIRED, SHALL BE FULL PENETRATION BUTT WELD.
10. ANY TEMPORARY STIFFENING STEEL WORK REQUIRED DURING FABRICATION, TRANSPORTATION OR ERECTION PURPOSES SHALL BE DESIGNED AND SUPPLIED BY THE CONTRACTOR, SUCH STEEL WORK SHALL BE REMOVED AND FLUE SURFACES MADE GOOD AFTER ERECTION.
11. TESTING OF WELDS UNLESS NOTED OTHERWISE ON THE DRAWINGS, SHALL BE AS FOLLOWS:
 - a) FILLET WELDS:
 - i) MACROETCH EXAMINATION ON PRODUCTION COUPONS.
 - ii) 100% DYE PENETRATION TEST/MAGNETIC PARTICLE TEST.
 - b) BUTT WELDS:
 - i) 100% DYE PENETRATION TEST AFTER BLACK GOUGING.
 - ii) 10% (FOR SHOP WELDS) AND 15% (FOR SITE WELDS) RADIOGRAPHY TEST. WHERE RADIOGRAPHY IS NOT POSSIBLE, ULTRASONIC TESTING WILL BE CARRIED OUT.
 - c) THE WELD RUN TO BE TESTED, SHALL BE EVENLY DISTRIBUTED OVER THE TOTAL LENGTH OF APPLICABLE WELDS ON EACH CAN.
 - d) THE PERCENTAGE OF WELDS TESTED SHALL BE INCREASED AS JUDGED NECESSARY BY THE ENGINEER-IN-CHARGE, BUT TO NOT LESS THAN 20% FOLLOWING IDENTIFICATION OF SIGNIFICANT DEFECTIVE WELDS AND ONLY REDUCED TO THE 10/15% NORM AFTER CONSISTENT QUALITY/INTEGRITY IS RE-ESTABLISHED.
12. WELDING OF TITANIUM PLATE SHALL BE DONE IN ACCORDANCE WITH TECHNICAL SPECIFICATION.
13. THE TERM 'SHOP' WELD REFERS TO ALL WELDS MADE DURING FABRICATION, OF INDIVIDUAL FLUE CANS AT FABRICATION YARD. 'SITE' WELD REFERS TO WELDS MADE DURING FLUE ERECTION FOR JOINING TOGETHER OF CANS WITHIN WIND FIELD.
14. FOR GENERAL NOTES AND DETAILING OF STEEL STRUCTURAL WORKS REFER DRG. NO. PE-DG-434-600-C002.
15. CONDENSATE COLLECTION CHANNEL SHALL BE WELDED WITH FLUE CAN AS APPLICABLE AS PER CONDENSATE FLUE STUDY. FOR DETAIL AND LOCATION OF CONDENSATE COLLECTION CHANNEL REFER SEPARATE DRG.



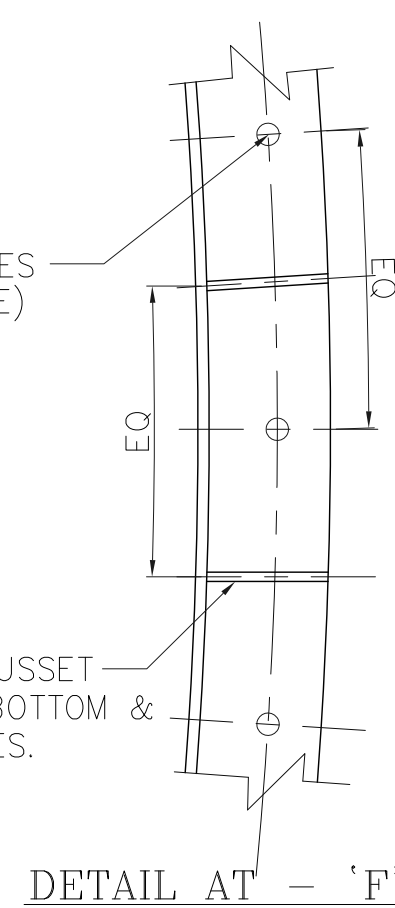
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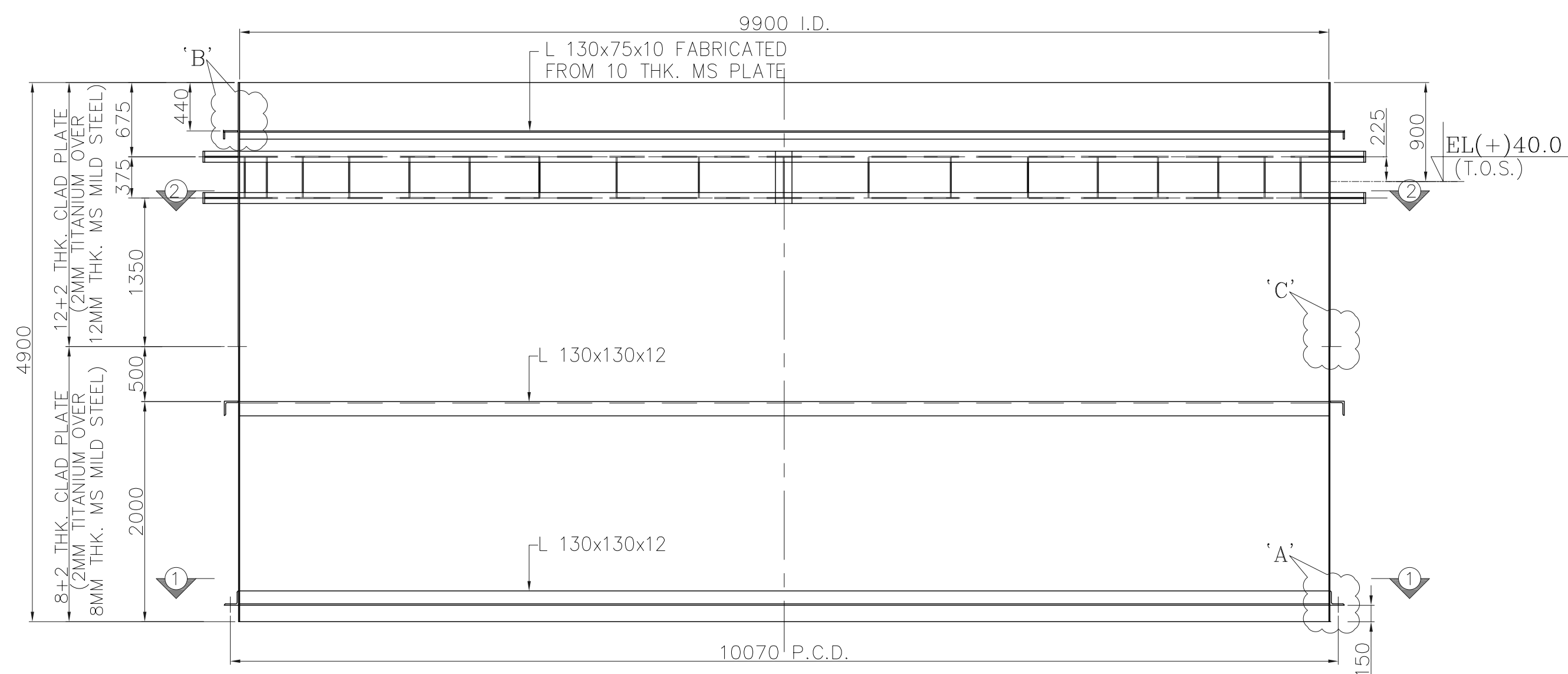
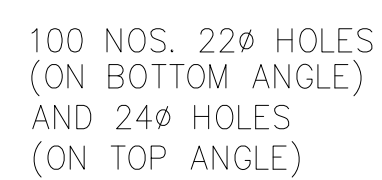
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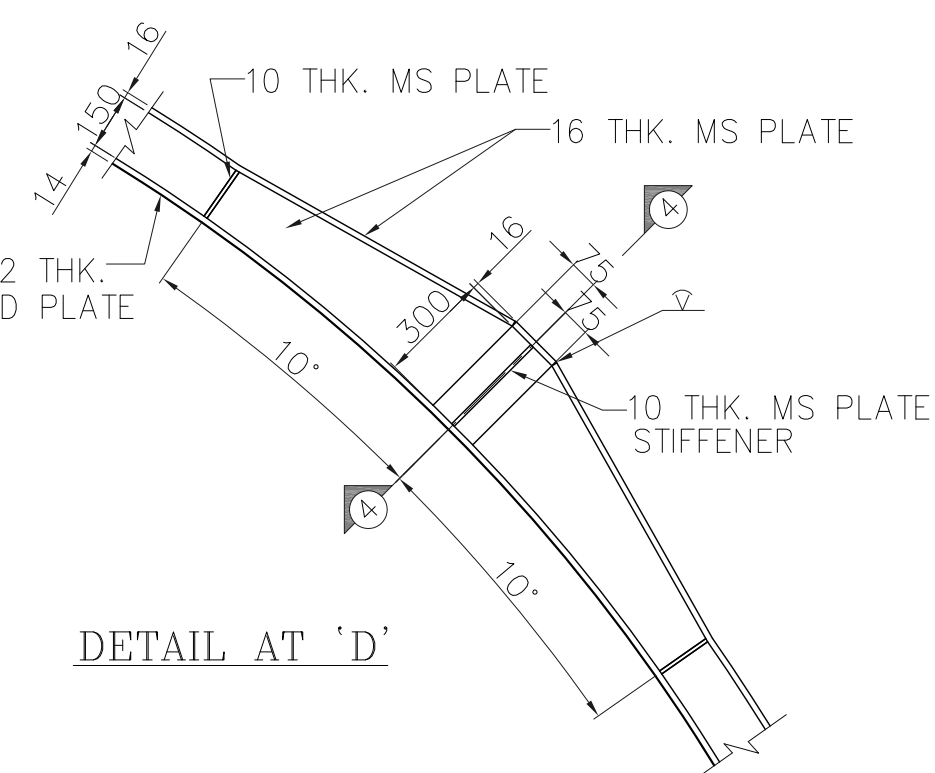
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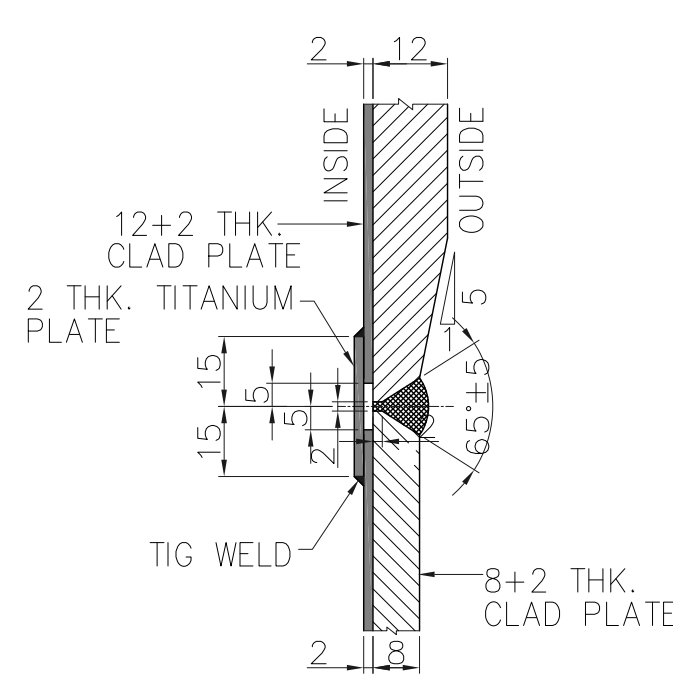
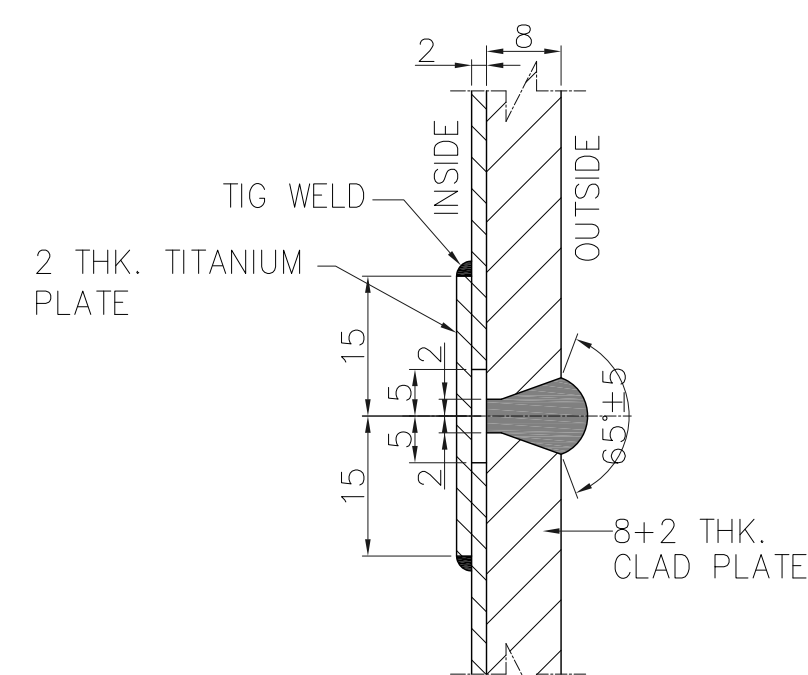
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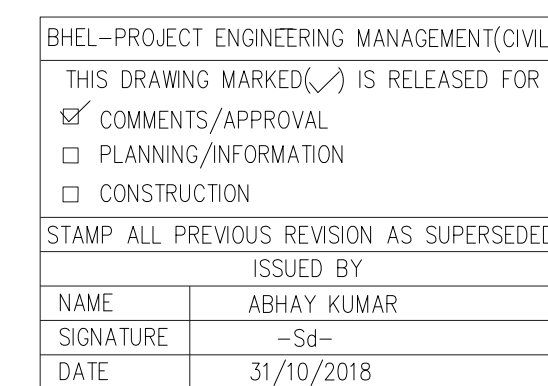
ELEVATION OF CAN TYPE 'E'



DETAIL AT 'D'

DETAIL AT 'C'

DETAIL AT - 'E'



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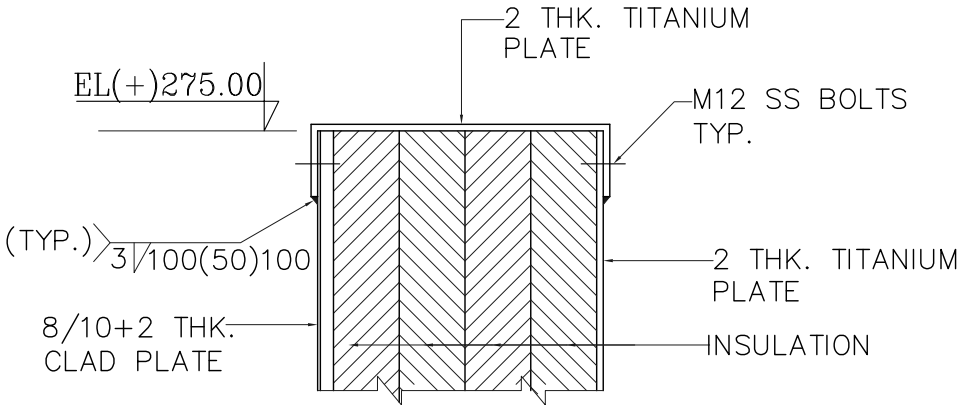
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CUSTOMER	NTPC LIMITED
3x800MW PATRATU SUPER THERMAL POWER PROJECT	

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DEPT C/O	<table style="width: 100%; border-collapse: collapse;"> <tr> <th style="width: 10%;">DEPT</th> <th style="width: 10%;">C/O</th> <th style="width: 40%;">NAME</th> <th style="width: 10%;">SIGN</th> <th style="width: 10%;">DATE</th> </tr> <tr> <td>DRN</td> <td>DEEPAK</td> <td></td> <td>—SD—</td> <td>31.10.2018</td> </tr> <tr> <td>ASN</td> <td>P. CHATTERJEE</td> <td></td> <td>—SD—</td> <td>31.10.2018</td> </tr> <tr> <td>CHD</td> <td>ABHAY</td> <td></td> <td>—SD—</td> <td>31.10.2018</td> </tr> <tr> <td>DEPT</td> <td>AKS</td> <td></td> <td>—SD—</td> <td>31.10.2018</td> </tr> </table>	DEPT	C/O	NAME	SIGN	DATE	DRN	DEEPAK		—SD—	31.10.2018	ASN	P. CHATTERJEE		—SD—	31.10.2018	CHD	ABHAY		—SD—	31.10.2018	DEPT	AKS		—SD—	31.10.2018
DEPT	C/O	NAME	SIGN	DATE																						
DRN	DEEPAK		—SD—	31.10.2018																						
ASN	P. CHATTERJEE		—SD—	31.10.2018																						
CHD	ABHAY		—SD—	31.10.2018																						
DEPT	AKS		—SD—	31.10.2018																						

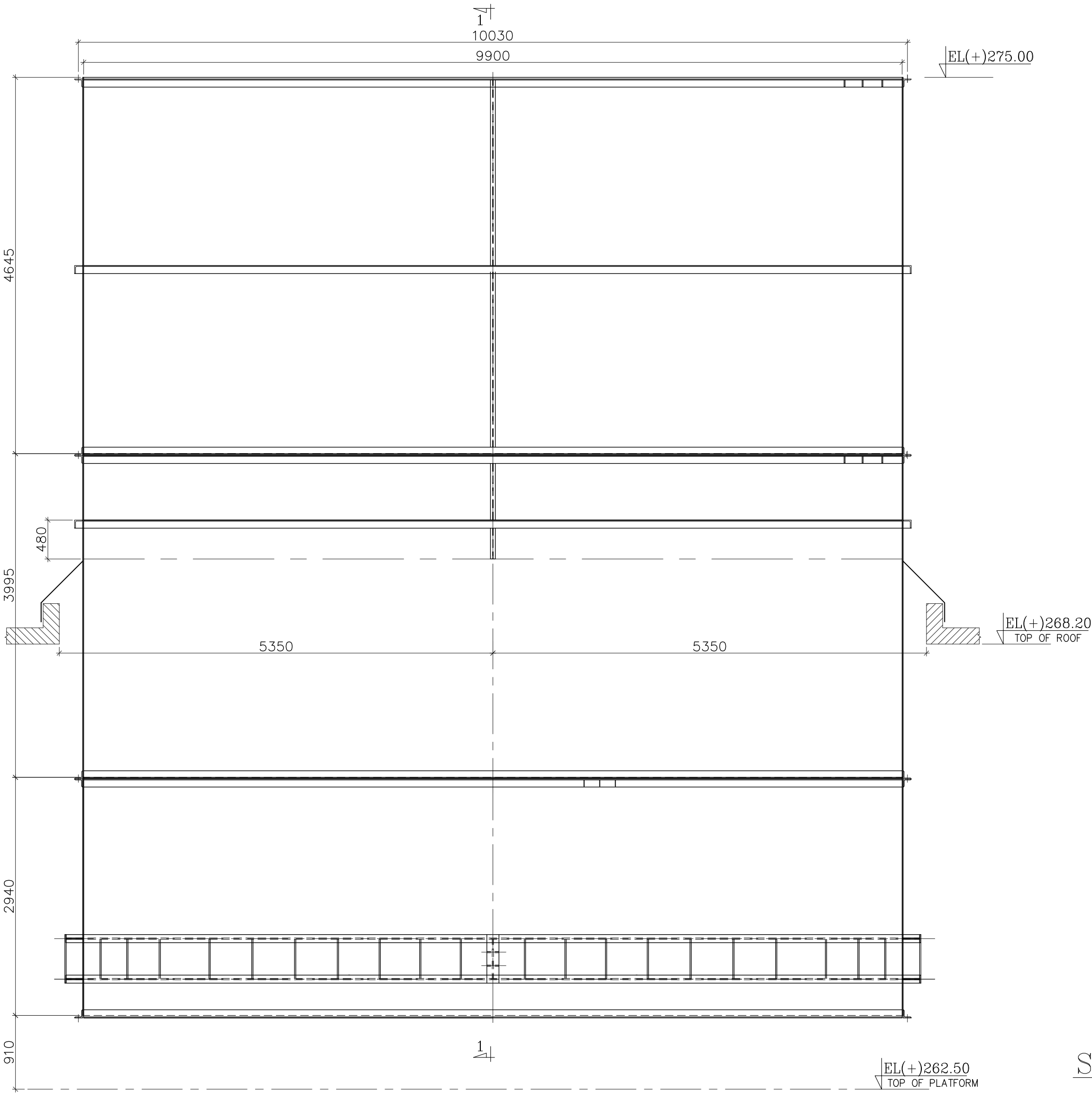
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				<u>LINER DETAILS- CAN TYPE E</u>			
				DEPT.	SCALE 1:100	DRAWING NO.	
				SKIN		PE-DG-434-620-C027	
						SHEET 1 OF 1	REV. 0

ANNEXURE-IV
PVUNL-2X800MW PATRATU STPP

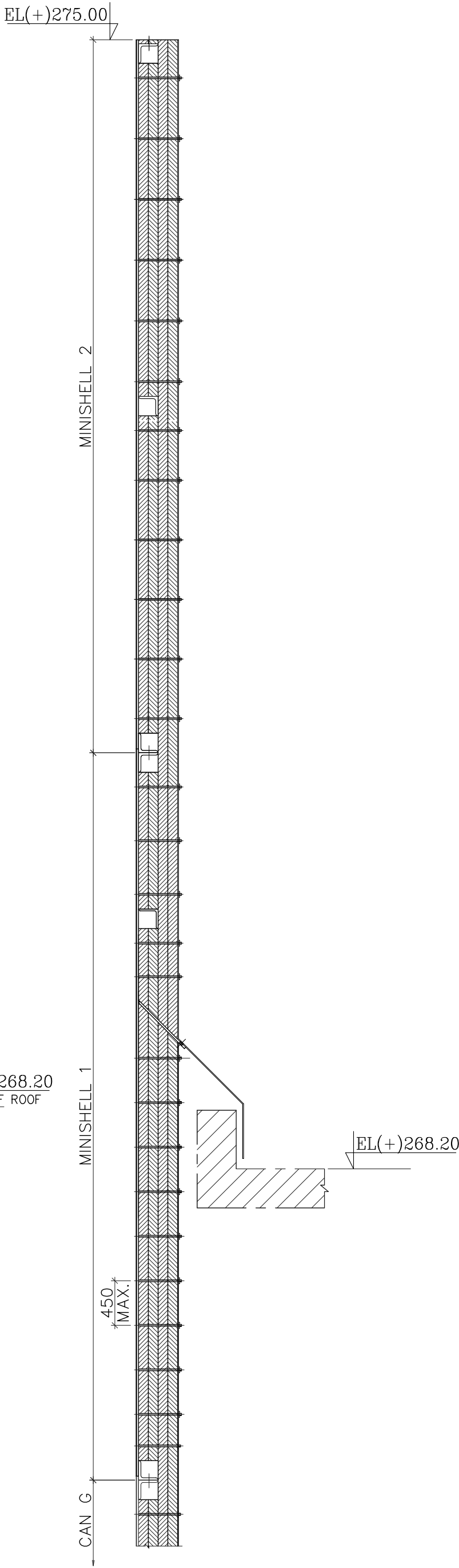
MINISHELL DETAILS



DETAIL AT 'A'

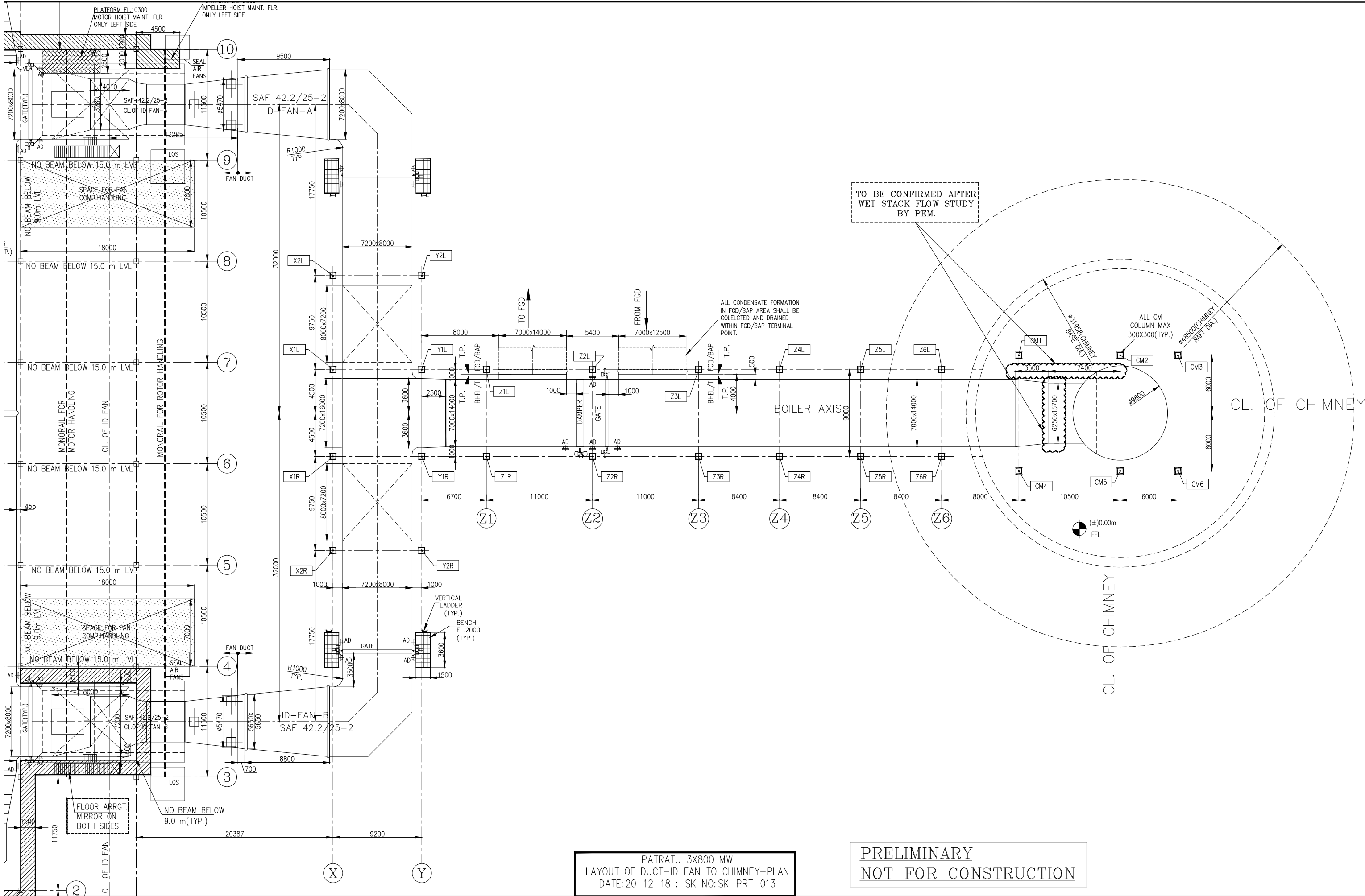


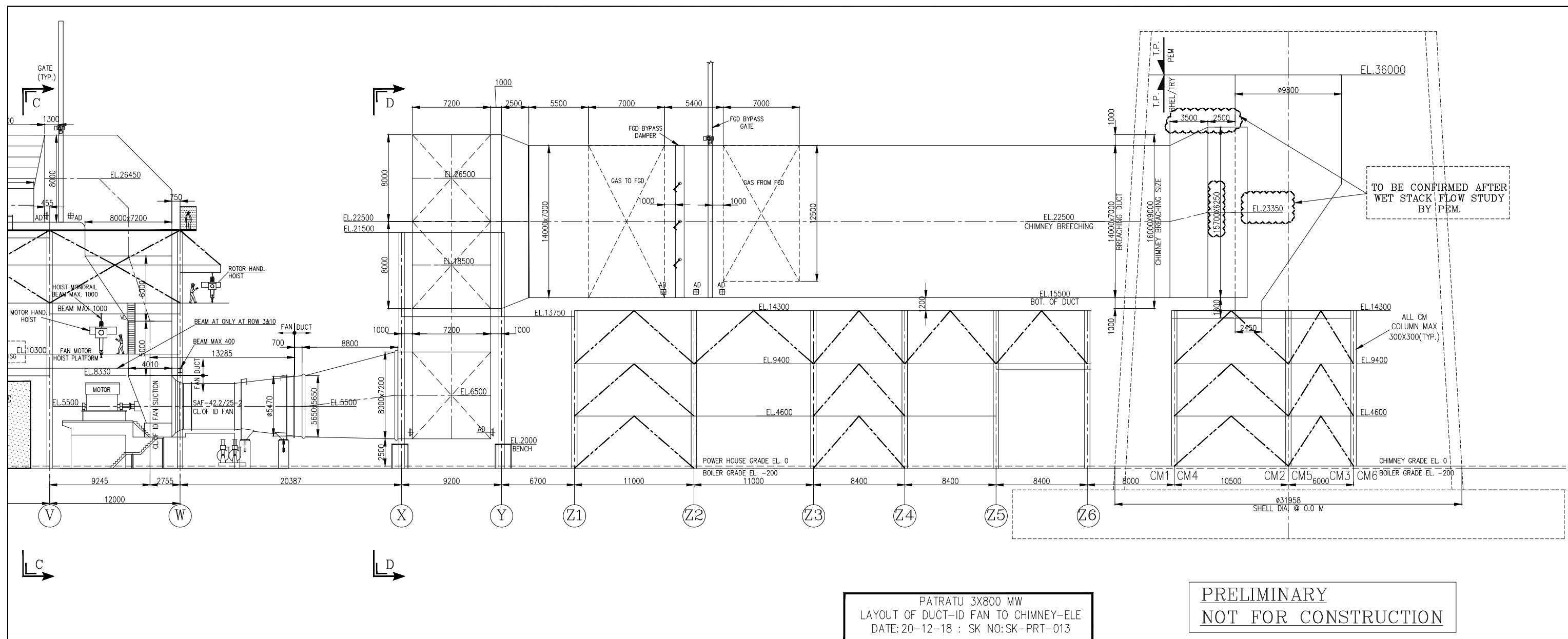
SECTION OF MINISHELL



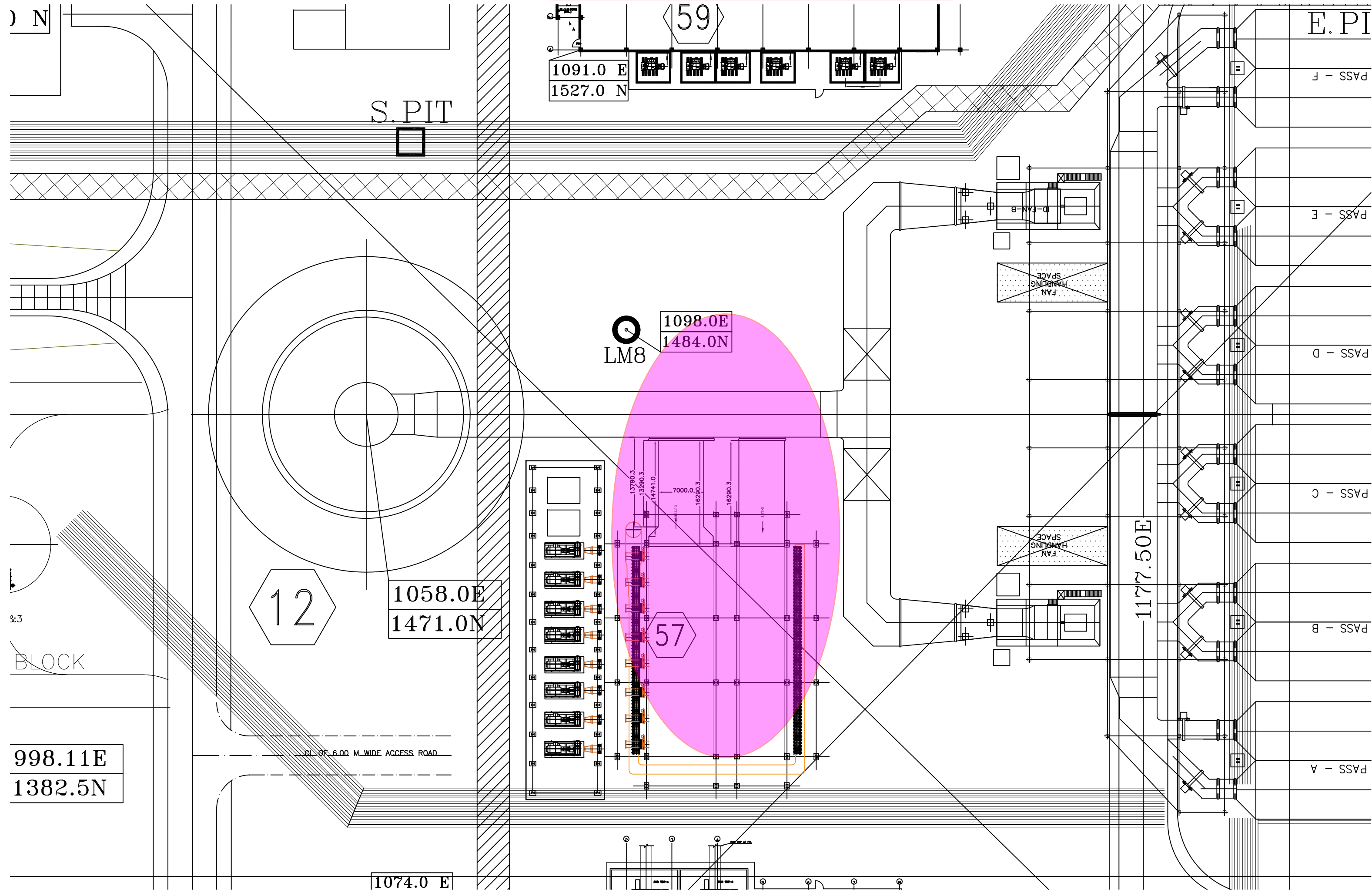
SECTION 1-1
SHOWING INSULATION FIXING

ANNEXURE-V-FGD LAYOUT

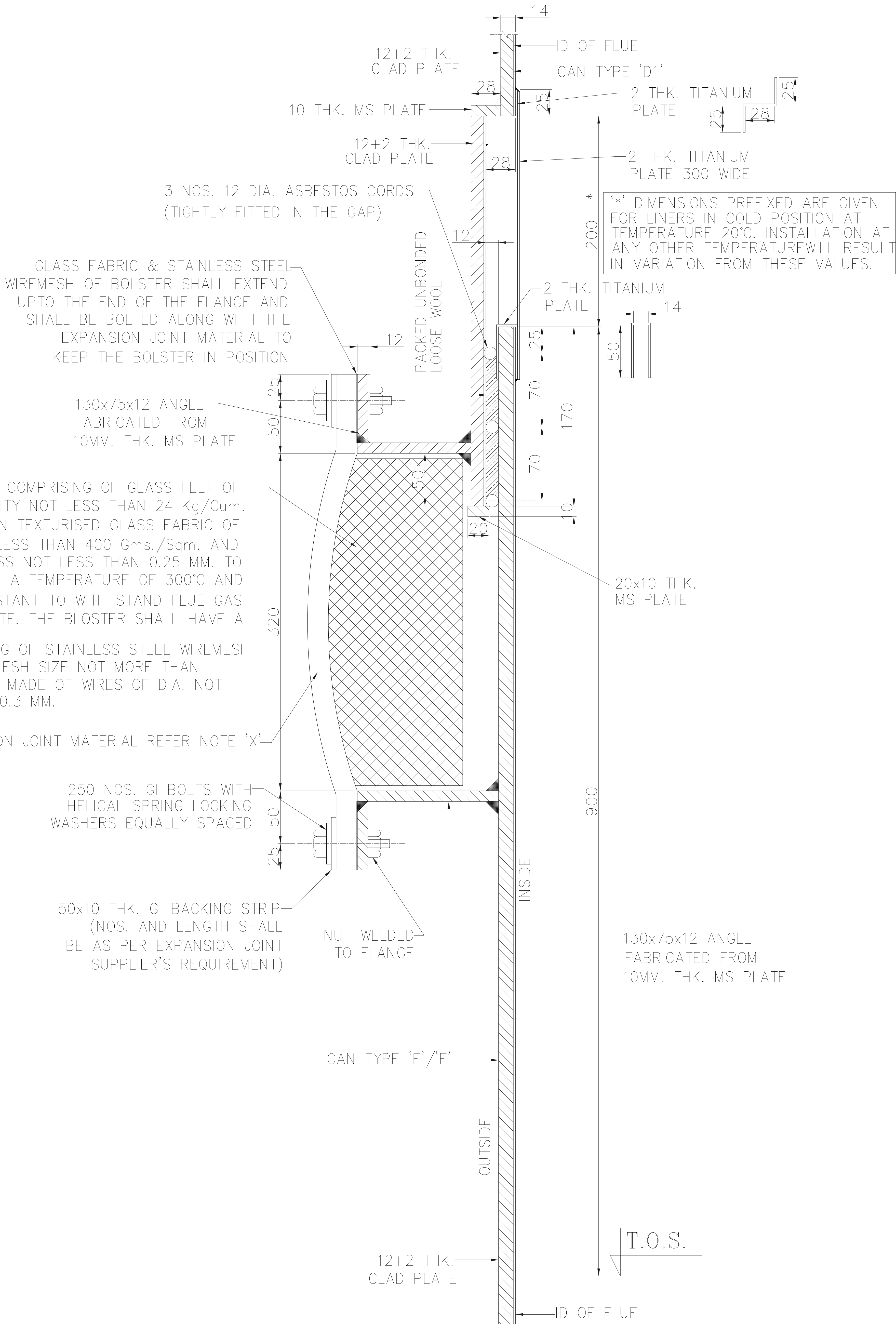




FGD OUTLET TO MAIN DUCT DETAILS



ANNEXURE-VI: EXPANSION JOINT



NOTES 'X'

1. THE EXPANSION JOINT SUPPLIER SHALL FULLY SATISFY HIMSELF ABOUT THE SATISFACTORY PERFORMANCE OF THE JOINT MATERIAL AS PER ACTUAL SITE CONDITION AND FLUE GAS PARAMETERS. THE SUPPLIER SHALL GET APPROVAL FOR SAME BEFORE INSTALLATION.
2. THE SUPPLIER SHALL GET APPROVAL FOR EXPANSION JOINT MATERIAL BEFORE INSTALLATION.
3. THE SUPPLIER SHALL ALSO PROVIDE AN INSTALLATION DISMANTLING AND MAINTENANCE USER HANDBOOK FOR THE EXPANSION COMPENSATOR
4. THE EXPANSION JOINT IN FLUE LINER SHALL COMPRISE OF NON METALLIC FLUOROELASTOMER MATERIAL SUITABLE TO WITHSTAND A TEMPERATURE OF 300° C AND SHALL BE ACID RESISTANT TO WITHSTAND FLUE GAS CONDENSATE ARISING OUT OF FLUE GAS.

NOTES:

1. ALL DIMENSIONS ARE IN MILLIMETRES & ELEVATIONS ARE IN METRES.
2. FASTENERS SHALL CONFIRM TO IS:1363.
3. FOR LAYOUT OF LINER CANS REFER DRG. NO. PE-DG-434-620-C022
4. THE VARIOUS LAYERS OF THE EXPANSION COMPENSATOR SHALL BE MANUFACTURED TO THE SPECIFIED THICKNESS AND UNIT WEIGHTS WITHIN A MANUFACTURING TOLERANCE OF 5% OF THE ABSOLUTE SPECIFIED VALUES.
5. THE MATERIAL SHALL BE TRANSPORTED, HANDLED, STORED, ETC. STRICTLY IN ACCORDANCE WITH THE SUPPLIER'S RECOMMENDATIONS.

BHEL-PROJECT ENGINEERING MANAGEMENT(CIVIL)	
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☐ CONSTRUCTION	
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ISSUED BY	
NAME	ABHAY KUMAR
SIGNATURE	-Sd-
DATE	20.11.2018

NTPC. DRAWING NO. - 9585-001-317-PVC-C-0581				
CUSTOMER				
NTPC LIMITED				
3x800MW PATRATU SUPER THERMAL POWER PROJECT				
Bharat Heavy Electricals Ltd POWER SECTOR PROJECT ENGINEERING MANAGEMENT NOIDA				
DEPT C	CODE DRN DESIGN	NAME P. CHATTERJEE	SIGN -Sd-	DATE 20.11.2018
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CHIMNEY DETAIL OF LINER EXPANSION JOINTS				
DRAWING NO. PE-DG-434-620-C028				
SHEET 1 OF 1 REV. 0				

JOB NO.	434
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SHEET	1	OF	1	REV.	0
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SIZE-A1

ANNEXURE-VII: WIND ROSE DIAGRAM
PVUNL-2X800MW PATRATU STPP

(PLANT NORTH)

N



NORTH



44°

NE

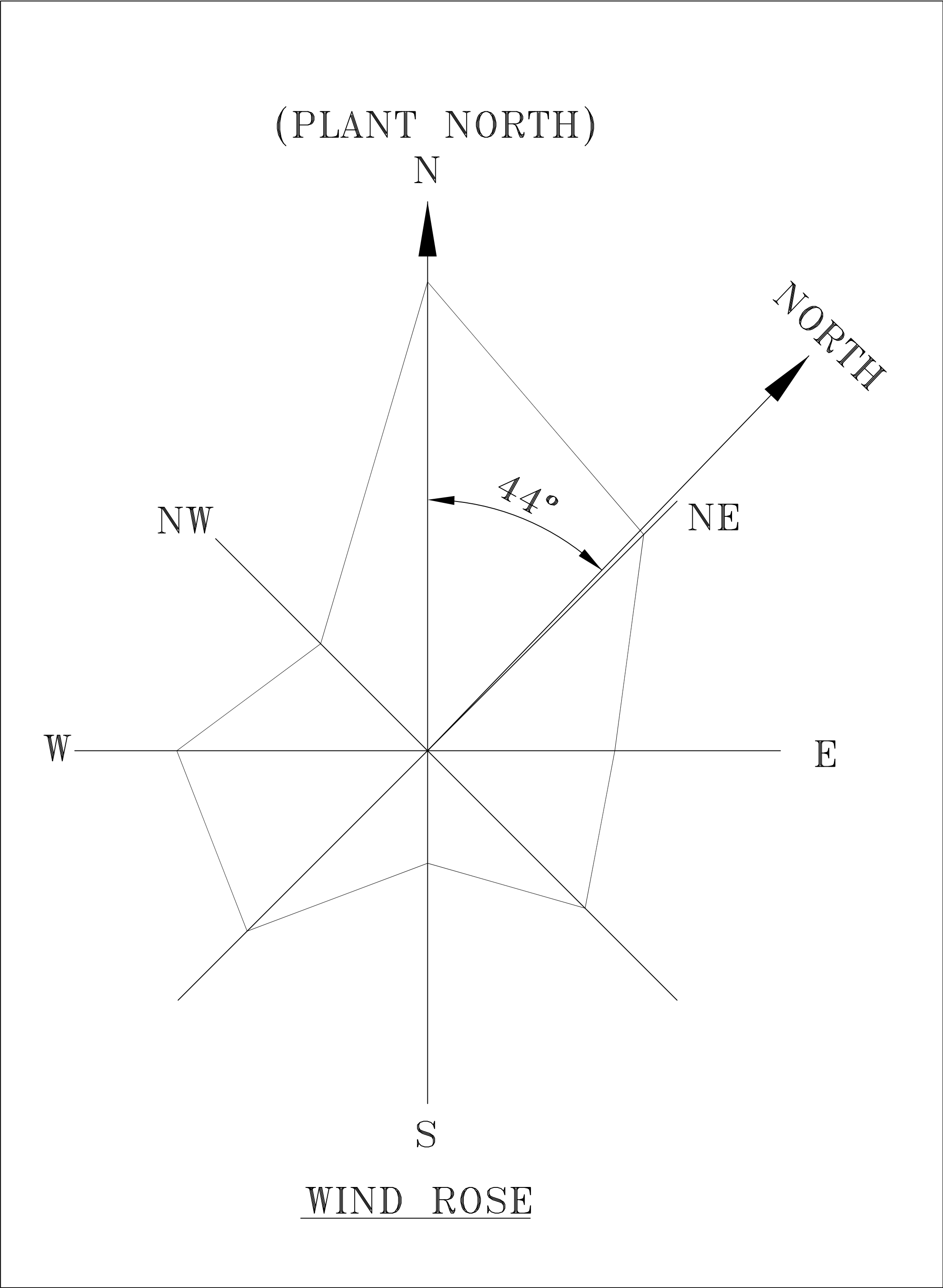
NW

W

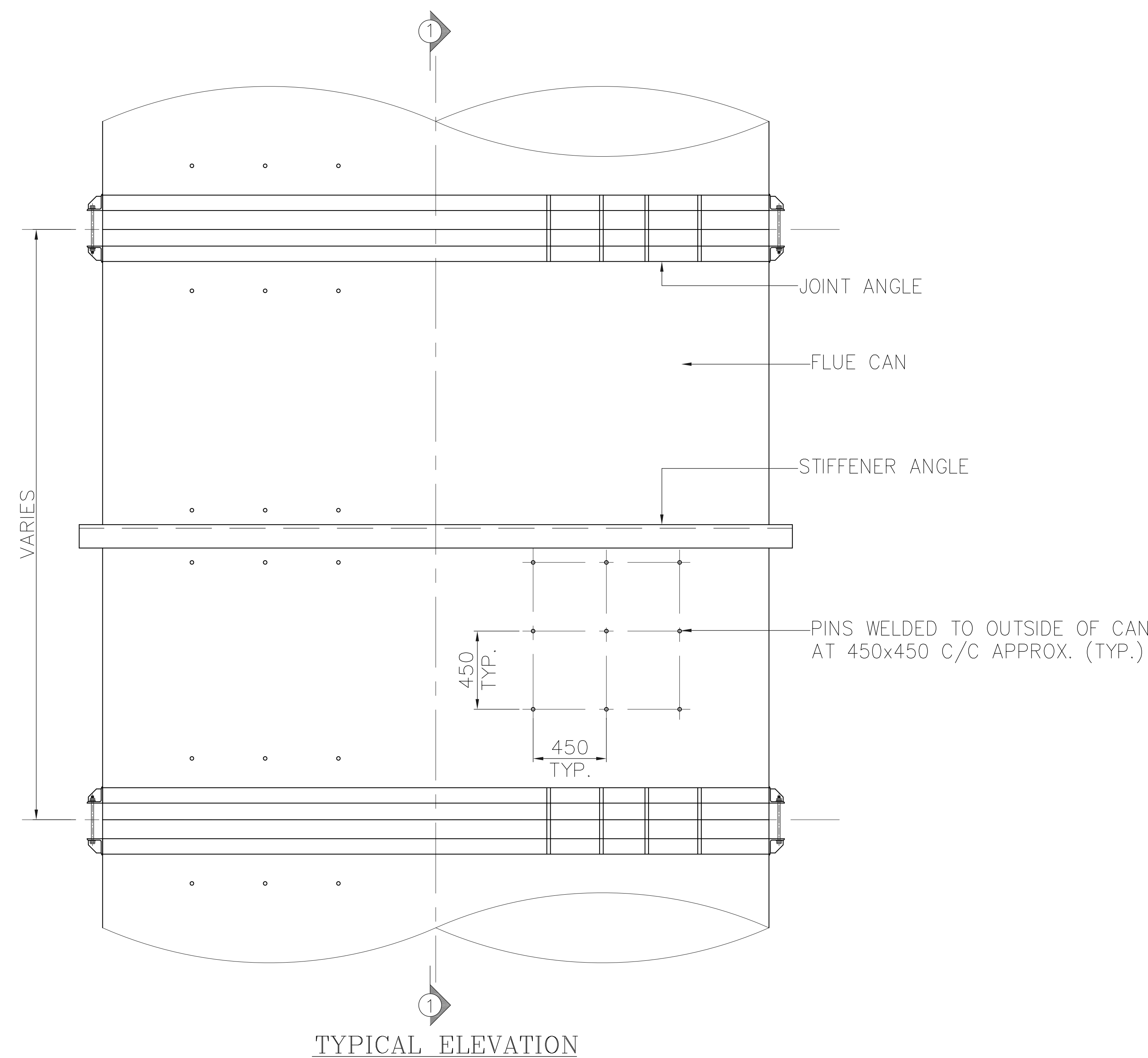
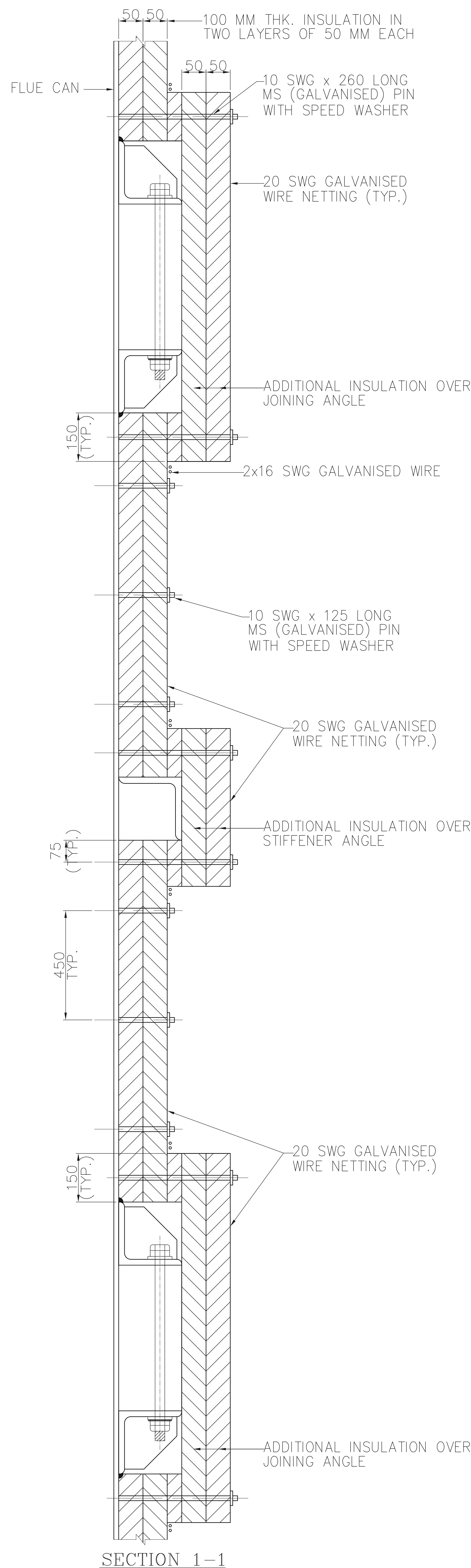
E

S

WIND ROSE



ANNEXURE-VII: FIXING DETAIL OF LINER INSULATION



NOTES:

1. ALL DIMENSIONS ARE IN MILLIMETRES AND LEVELS ARE IN METRES.
2. FLUE INSULATION SHALL BE OF RESIN BONDED ROCK WOOL SLABS OF DENSITY 100 Kg/Cum
MAXIMUM THERMAL CONDUCTIVITY SHALL BE 0.52 mW/cm °c CONFORMING TO IS:819 AND
IS:8183.
3. FIXING OF ALL INSULATION TO ALL THE CANS SHALL AS DEFINED IN SPECIFICATION AND AS
SHOWN IN RELEVANT DRAWINGS.
4. INSULATION SHALL BE KEPT DRY ON SITE AND IN PARTICULAR SHALL REMAIN DRY AT ALL
TIMES IN PLACE ON FLUE CANS.

SPECIAL NOTE

DRAWINGS / DOCUMENTS ARE BEING SUBMITTED FOR INFORMATION.
BHEL HEREBY CONFIRMS FULL COMPLIANCE TO ALL THE SPECIFIED REQUIREMENTS OF THE CONTRACT SPECIFICATION, WITHOUT ANY DEVIATION, WHATSOEVER. IN CASE DURING THE TENURE OF THE CONTRACT, IT IS OBSERVED/FOUND THAT THE DATA/ INFORMATION IN THE RELEASED DRAWING/DOCUMENT IS NOT MEETING THE CONTRACT SPECIFICATION, BHEL/ITS VENDOR(S) WILL MODIFY/ RECTIFY/REPLACE THE SAME TO MEET THE SPECIFICATION WITHOUT ANY COMMERCIAL IMPLICATION OR ANY TIME EXTENSION TO PVUNL/NTPC IN THIS REGARD.

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DATE	31/01/2019

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12					14				15

NTPC. DRAWING NO. — 9585-001-317-PVC-C-0578	
CUSTOMER (PVC C-0578) NTPC	NTPC LIMITED
3x800MM PATRATU SUPER THERMAL POWER PROJECT	
OFFICE USE ONLY NTPC NTPC Limited Patratu	BHARAT HEAVY ELECTRICALS LTD POWER SECTOR PROJECT ENGINEERING MANAGEMENT Noida
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TITLE CHIMNEY FIXING DETAIL OF LINER INSULATION	
DEPT. SCALE : 1:50 SIGN	DRAWING NO. : PG-DC-434-C-0029 SHEET : 1 OF 1